

# Cosintering the Anode Active Material with $\text{Li}_7\text{La}_3\text{Zr}_2\text{O}_{12}$ Solid Electrolyte for the All-Solid-State Battery: How to Predict the Interfacial Reaction at Elevated Temperatures

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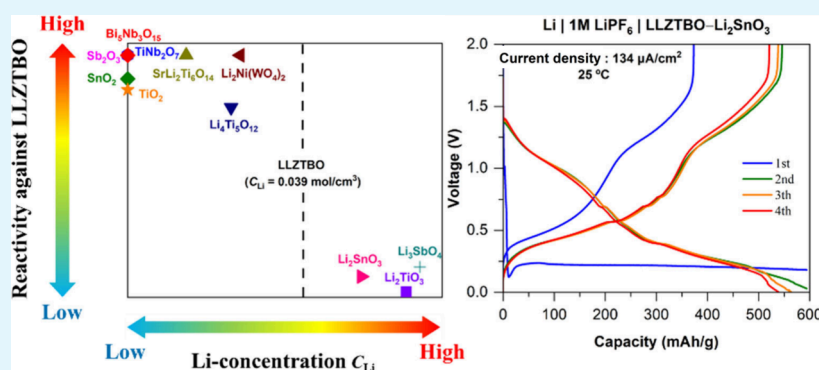
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**ABSTRACT:** Cosintered-type all-solid-state batteries composed of  $\text{Li}_7\text{La}_3\text{Zr}_2\text{O}_{12}$  (LLZ) have garnered significant attention as next-generation batteries that offer both high energy density and long cycle life. However, achieving low-resistance interfaces through cosintering of electrode materials, particularly between the anode active material and LLZ, remains a big challenge due to the formation of reaction phases caused by interdiffusion during high-temperature sintering. In this study, we demonstrated the lithium concentration within the materials ( $C_{\text{Li}}$ ; mol/cm<sup>3</sup>) as a key factor for predicting the reactivity between the anode active material and LLZ during high-temperature sintering. Various kinds of anode active materials with different  $C_{\text{Li}}$  values were mixed with LLZ, and the reactivity during sintering at 850 °C was carefully investigated. XRD results show that interfacial reaction proceeds between LLZ and low  $C_{\text{Li}}$  materials due to the occurrence of Li loss in LLZ. Contrarily,  $\text{Li}_2\text{SnO}_3$ ,  $\text{Li}_2\text{TiO}_3$ , and  $\text{Li}_3\text{SbO}_4$  in the high  $C_{\text{Li}}$  group (larger than that of LLZ) achieve interaction suppression against the LLZ electrolyte during high-temperature sintering. However, lattice parameter characterization and TEM images reveal that interdiffusion and side reactions occurred at the interface layer in the composite LLZ/high  $C_{\text{Li}}$  material. Densified composite LLZTBO– $\text{Li}_2\text{SnO}_3$  (relative density ~ 89%) and LLZTBO– $\text{Li}_2\text{TiO}_3$  pellets (~95%) were successfully obtained under 900 °C sintering for 15 h. Charge–discharge tests using the half-cell assembled with the cosintered composite anode and liquid electrolyte reveal the superior capacity of 550 mAh/g with nearly 92% Coulombic efficiency for the LLZTBO– $\text{Li}_2\text{SnO}_3$  cosintered anode. The approach reported herein has the potential to rapidly screen possible cosintered electrodes for garnet-type solid-state electrolytes and achieve cosintered-type all-solid-state batteries with high energy density.

**KEYWORDS:** Anode, Garnet-type LLZ, Cosintered, All-solid-state, Lithium battery

## 1. INTRODUCTION

In recent years, lithium-ion batteries (LiBs) have been regarded as the most widely used energy storage system (ESS) in several fields, including electric vehicles (EVs), isolated energy storage devices, and portable devices such as smartphones and laptops.<sup>1</sup> However, with the development of advanced rechargeable batteries, LiBs have faced several critical issues regarding energy density and safety. The incompatibility between the liquid electrolyte and highly advanced cathode and anode materials limits LiBs from meeting the future needs of rechargeable batteries. Moreover, the flammability of liquid LiBs also poses a safety hazard.<sup>2–5</sup>

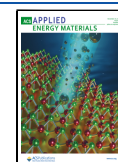
Solid-state electrolytes (SSEs) are considered good alternatives to conventional batteries based on liquid electrolytes due to their advantages, including a wide electrochemical window, strong mechanical, thermal, chemical, and electrochemical stability, and high ionic conductivity.<sup>6–9</sup> The family of SSEs, including solid polymer electrolytes,<sup>10</sup> inorganic oxide

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electrolytes,<sup>11–13</sup> inorganic sulfide electrolytes,<sup>14</sup> and others such as metal–organic frameworks,<sup>15</sup> has been widely investigated in recent years. Among them, garnet-type SSEs have emerged as one of the most promising and vital candidates due to their high ionic conductivity ( $10^{-4}$ – $10^{-3}$  S/cm), good chemical stability against Li-metal, wide potential window (0–9 V), and negligible electronic transport.<sup>16–19</sup>

In 2007,  $\text{Li}_7\text{La}_3\text{Zr}_2\text{O}_{12}$  (LLZ), with a high Li-ionic conductivity of  $3 \times 10^{-4}$  S/cm, was successfully prepared for the first time by sintering at 1230 °C for 36 h.<sup>20</sup> Since LLZ garnet-based electrolytes provide significant advantages in ionic conductivity, safety, chemical, thermal, and electrochemical stability, as well as air stability, extensive research has been carried out on the LLZ-based all-solid-state lithium batteries (ASSLBs). LLZ is reported to have tetragonal phases (space group  $I4_1/acd$ ) and cubic phases (space groups  $Ia\bar{3}d$  and  $I43d$ ). The conductivity of the cubic phase is more than 2 orders of magnitude higher than that of the tetragonal phase, and it is stable at high temperatures.<sup>21</sup> Therefore, numerous doping strategies have emerged to stabilize the cubic phases at room temperature, including  $\text{Ga}^{3+}$ ,  $\text{Al}^{3+}$ , or  $\text{Ge}^{3+}$  doped into the Li-sites<sup>22–27</sup> or  $\text{Ta}^{5+}$ ,  $\text{Gd}^{3+}$ ,  $\text{Te}^{5+}$ ,  $\text{Mo}^{6+}$ ,  $\text{Ce}^{4+}$ ,  $\text{Nb}^{5+}$ ,  $\text{Sb}^{5+}$ , or  $\text{Bi}^{5+}$  into the Zr-sites.<sup>28–37</sup> In addition, to obtain dense pellets and high ionic conductivity of LLZ, sintering at a temperature over 1000 °C is essential to reduce grain boundary resistance.<sup>38–43</sup>

For various ASSLBs operations, forming a composite electrode (CE) via mixing an active material and SSE, followed by a cosintering process, is a suitable approach to lower the interfacial resistance and facilitate fast Li-ion transportation by providing a continuous pathway. Hence, the electrochemical and chemical interactions between LLZ and an electrode material should be considered to be significant factors. High-temperature sintering may form a highly resistive interface phase due to interdiffusion and unexpected reactions between the LLZ and the electrode material, resulting in poor battery performance.

To prevent the interfacial reaction caused by sintering at high temperatures above 1000 °C, it is crucial to lower the sintering temperature to a range stable for coexisting SSEs and active materials thermodynamically.<sup>44,45</sup> In recent years, various cathode materials, such as  $\text{LiCoO}_2$ ,<sup>46</sup> have been investigated for use in a cosintering type of cathode with a solid-state electrolyte. Our group has reported that Bi substitution and composition control can significantly reduce the sintering temperature of LLZ, allowing it to be cosintered with  $\text{LiCoO}_2$ .<sup>47–50</sup> However, there are still few reports on viable anode materials for LLZ, and the selection of anode materials applicable to LLZ-based ASSLBs has yet to progress. To date, the most widely used anode for an LLZ-based electrolyte is Li-metal. Although Li-metal exhibits ultrahigh specific capacity (3860 mAh/g) and a large negative potential of  $-3.04$  V,<sup>51</sup> high interfacial resistance and the growth and expansion of Li dendrites remain significant challenges and are unsolved.<sup>52–55</sup>

In this study, we aimed to explore the anode materials that can be cosintered with the LLZ-based electrolyte. In the case of anode materials, achieving both reaction suppression during sintering and high energy density is essential. Candidates including  $\text{SnO}_2$ ,  $\text{TiO}_2$ ,  $\text{Sb}_2\text{O}_3$ ,  $\text{TiNb}_2\text{O}_7$ ,  $\text{Bi}_5\text{Nb}_3\text{O}_{15}$ ,  $\text{SrLi}_2\text{Ti}_6\text{O}_{14}$ ,  $\text{Li}_2\text{Ni}(\text{WO}_4)_2$ ,  $\text{Li}_2\text{SnO}_3$ ,  $\text{Li}_2\text{TiO}_3$ , and  $\text{Li}_3\text{SbO}_4$  have been chosen. The reaction between varied materials is generally predictable from thermodynamic calculations,

because it proceeds when  $\Delta G^\circ$  is negative. Moreover, the reaction kinetics determine the progress of the reaction. Chemical potential ( $\mu$ ) difference could be regarded as a significant driving force of interdiffusion. However, calculating the chemical potential of Li for many materials requires significant time and cost. Herein, we attempted to simplify “ $\mu$ ” to “Li-concentration ( $C_{\text{Li}}$ : mol/cm<sup>3</sup>)” in the LLZ/anode cosintered system, because  $C_{\text{Li}}$  can be easily estimated from crystallographic databases. Therefore, the relationship between  $C_{\text{Li}}$  of electrode materials and the reactivity of the LLZ was investigated. The information on the  $C_{\text{Li}}$  of anode candidates is shown in Table 1. Ideally, the electrode materials should not

**Table 1. Lithium Concentration of Anode Candidates and SSEs**

Material	Li-concentration $C_{\text{Li}}$ [mol/cm <sup>3</sup> ]
$\text{SnO}_2$	0
$\text{TiO}_2$	0
$\text{Sb}_2\text{O}_3$	0
$\text{TiNb}_2\text{O}_7$	0
$\text{Bi}_5\text{Nb}_3\text{O}_{15}$	0
$\text{SrLi}_2\text{Ti}_6\text{O}_{14}$	0.014
$\text{Li}_2\text{Ni}(\text{WO}_4)_2$	0.025
$\text{Li}_4\text{Ti}_5\text{O}_{12}$	0.030
$\text{Li}_{6.5}\text{La}_3\text{Zr}_{1.5}\text{Ta}_{0.3}\text{Bi}_{0.2}\text{O}_{12}$ (LLZTBO)	0.039
$\text{Li}_2\text{SnO}_3$	0.055
$\text{Li}_2\text{TiO}_3$	0.062
$\text{Li}_3\text{SbO}_4$	0.065

react with LLZ at elevated temperatures and should also be densified simultaneously to create a suitable interface for Li-ion conduction. Thus, in this study, to justify suitable materials for cosintering with LLZ, the crystal structure change and sintering properties were investigated in detail.

## 2. EXPERIMENTAL SECTION

### 2.1. Synthesis of LLZ-Based Electrolytes.

$\text{Li}_{6.5}\text{La}_3\text{Zr}_{1.5}\text{Ta}_{0.3}\text{Bi}_{0.2}\text{O}_{12}$  (LLZTBO) compounds were synthesized through a conventional solid-state reaction (SSR).  $\text{Li}_2\text{CO}_3$  (>99.99%; Rare Metallic Co., Ltd., Japan),  $\text{La}(\text{OH})_3$  (>99.9%; Sigma-Aldrich, Germany),  $\text{ZrO}_2$  (>98%; Kojundo Chemical Laboratory Co., Ltd., Japan),  $\text{Bi}_2\text{O}_3$  (>98%; Sigma-Aldrich, Germany), and  $\text{Ta}_2\text{O}_5$  (>99.9%; FUJIFILM Wako Pure Chemical Corporation, Japan) were used as starting materials. 2% excess of  $\text{Li}_2\text{CO}_3$  and stoichiometric ratio of the remaining starting materials were weighted and mixed by ball-milling in 2-propanol using 3 mm diameter of Tungsten balls for 20 h. After full evaporation of the solvent, the mixtures were ground in 2-propanol for 30 min. The samples were then dried at 105 °C for 2 h and calcined in an alumina crucible at 800 °C for 15 h with a ramp rate of 400 °C/h. After calcination, to obtain a small particle size, the resultant powders were repeatedly ground for 15 min and then ball-milled in 2-propanol for 900 min, and this was repeated 2 times. The resulting samples were then fully dried, ground, and used for further research.

**2.2. Synthesis of Anode Candidates.**  $\text{SnO}_2$  (>99.9%; Kojundo Chemical Laboratory Co., Ltd., Japan),  $\text{TiO}_2$  (>99.8%; FUJIFILM Wako Pure Chemical Corporation, Japan), and  $\text{Sb}_2\text{O}_3$  (>99.9%; FUJIFILM Wako Pure Chemical Corporation, Japan) were directly used as anode candidates. All of the remaining anode candidates, including  $\text{Bi}_5\text{Nb}_3\text{O}_{15}$ ,  $\text{TiNb}_2\text{O}_7$ ,  $\text{SrLi}_2\text{Ti}_6\text{O}_{14}$ ,  $\text{Li}_2\text{Ni}(\text{WO}_4)_2$ ,  $\text{Li}_2\text{SnO}_3$ ,  $\text{Li}_2\text{TiO}_3$ , and  $\text{Li}_3\text{SbO}_4$ , were prepared using a conventional SSR, with weights in stoichiometric ratios with an excess of  $\text{Li}_2\text{CO}_3$  additive. All the precursor materials were mixed by ball-milling in 2-propanol using zirconia balls of 1 mm diameter for 15 h. After evaporation of the solvent, the mixtures were calcinated and placed on a Au sheet under

different conditions. The resultant samples were subsequently ground for 15 min. The information on starting materials, excess of Li source, and calcination conditions are shown in Table S1.

**2.3. Preparation of Composite Pellets (CPs).** Each anode candidate and LLZTBO were mixed in a weight ratio of 1:1 in 2-propanol through uniaxial ball-milling at 625 rpm for 15 h, separately. After proper mixing, the mixtures were dried and pressed into pellets (0.2 g) through uniaxial pressing under a pressure of 1.5 MPa and subsequent Cold Isostatic Pressing at 360 kgf/cm. Thereafter, those CPs were sintered at 850 °C for 5 h with a ramp rate of 5 °C/min. An Au sheet was placed on the bottom of the pellets to prevent Al contamination from the alumina setter.

**2.4. Material Characterization.** Crystal structure and phase identification of each CP were conducted by X-ray diffraction (XRD) using a SmartLab device (Rigaku, Japan) with Cu K $\alpha$  radiation. Element distribution was probed by transmission electron microscopy (TEM) (JEM-ARM200F, JEOL, Japan). Relative densities were calculated from the bulk and theoretical densities. Lattice parameters were refined by Rietveld analysis using PDXL2 software (Rigaku, Japan). Impurity ratio  $R_i$  of each anode candidate could be calculated through Equation 1:

$$R_i = \frac{n(\text{Total Reflections associated to Impurity phases})}{n(\text{All diffraction peaks})} \times 100\% \quad (1)$$

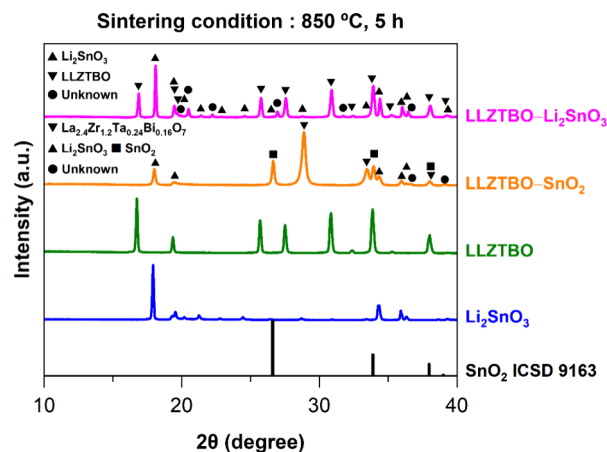
To reveal the sintering behavior of the composite pellets, typical samples were cosintered at different temperatures for 5 h at a constant heating rate of 5 °C/min.

**2.5. Electrical Characterization.** The electrode performance of a typical composite LLZ/anode dense electrode was measured through a liquid-electrolyte based half-cell: Li|1 M LiPF<sub>6</sub> (EC: DEC = 1:2 (vol %))|composite LLZ/anode. The CPs were polished to a thickness of 200  $\mu\text{m}$  with sandpaper (Grit 600). The Pt film was sputtered on the surface of the CPs as a current collector. A glass microfiber filter ( $\Phi$ 21 mm, Whatman GF/A) was used as a separator. The half-cells were cycled galvanostatically between 0 and 2 V at room temperature by using a battery test system (HJ1020mSD8, Hokuto Denko, Japan).

### 3. RESULTS AND DISCUSSION

**3.1. Relationship between  $C_{\text{Li}}$  in the Electrode Materials and the Reactivity of LLZTB.** Anode active materials, including SnO<sub>2</sub>, TiO<sub>2</sub>, Sb<sub>2</sub>O<sub>3</sub>, TiNb<sub>2</sub>O<sub>7</sub>, Bi<sub>5</sub>Nb<sub>3</sub>O<sub>15</sub>, SrLi<sub>2</sub>Ti<sub>6</sub>O<sub>14</sub>, and Li<sub>2</sub>Ni(WO<sub>4</sub>)<sub>2</sub>, the  $C_{\text{Li}}$  values of which are smaller than that of LLZTB, are defined as the low  $C_{\text{Li}}$  group. Contrarily, Li<sub>2</sub>SnO<sub>3</sub>, Li<sub>2</sub>TiO<sub>3</sub>, and Li<sub>3</sub>SbO<sub>4</sub>, the  $C_{\text{Li}}$  of which are higher than that of LLZ, are classified in the high  $C_{\text{Li}}$  group. SnO<sub>2</sub> has been widely reported as an anode for lithium batteries.<sup>56</sup> In addition, Li<sub>2</sub>SnO<sub>3</sub> has attracted considerable attention as an anode for Li-ion battery due to the theoretical capacity of tin being as high as 993 mAh/g.<sup>57</sup> Herein, SnO<sub>2</sub> (Low  $C_{\text{Li}}$  group) and Li<sub>2</sub>SnO<sub>3</sub> (High  $C_{\text{Li}}$  group) were presented as a typical comparative group. TiO<sub>2</sub>/Li<sub>4</sub>Ti<sub>5</sub>O<sub>12</sub>/Li<sub>2</sub>TiO<sub>3</sub> is an additional comparative group presented below.

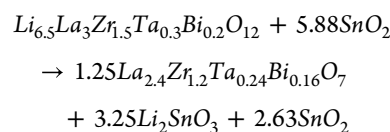
XRD patterns of synthesized Li<sub>2</sub>SnO<sub>3</sub>, composite LLZTBO–SnO<sub>2</sub>, and LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> pellets are shown in Figure 1. As can be seen, for the LLZTBO–SnO<sub>2</sub> composite pellets, the diffraction peaks of LLZTBO completely disappeared, whereas the presence of Li<sub>2</sub>SnO<sub>3</sub>, SnO<sub>2</sub>, La<sub>2.4</sub>Zr<sub>1.2</sub>Ta<sub>0.24</sub>Bi<sub>0.16</sub>O<sub>7</sub>, and unknown impurities could be observed after cosintering at 850 °C for 5 h, indicating an extremely weak chemical stability of LLZTBO against low  $C_{\text{Li}}$  substance SnO<sub>2</sub>. The impurity ratio  $R_i$  of SnO<sub>2</sub> is about 90%. Nevertheless, a cosintered LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> composite pellet was successfully prepared under the same sintering conditions. As seen in Figure 1, the diffraction peaks of LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> could be clearly distinguished as Li<sub>2</sub>SnO<sub>3</sub>



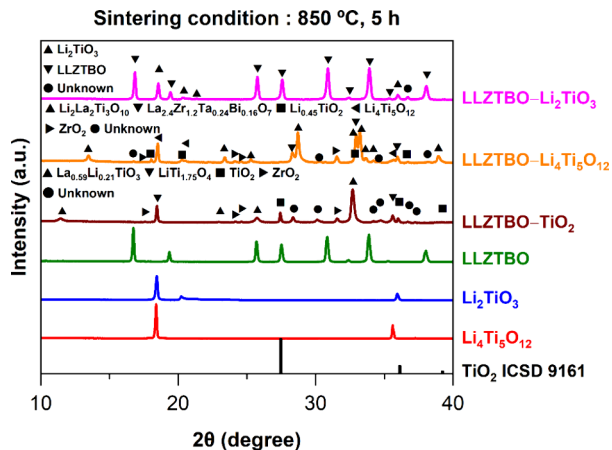
**Figure 1.** XRD patterns of synthesized Li<sub>2</sub>SnO<sub>3</sub>, LLZTBO–SnO<sub>2</sub>, and LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> pellets.

and LLZTBO, while a few unknown impurity phase peaks of 9% appear.

It has been reported that fluorite-type La<sub>2.4</sub>Zr<sub>1.2</sub>Ta<sub>0.4</sub>O<sub>7</sub> is a precursor oxide for low-temperature formation of garnet-type Li<sub>6.5</sub>La<sub>3</sub>Zr<sub>1.5</sub>Ta<sub>0.5</sub>O<sub>12</sub>.<sup>58</sup> Therefore, in view of the huge difference of  $C_{\text{Li}}$  between SnO<sub>2</sub> (0 mol/cm<sup>3</sup>) and LLZTBO (0.039 mol/cm<sup>3</sup>), we could speculate that the diffraction peak of La<sub>2.4</sub>Zr<sub>1.2</sub>Ta<sub>0.24</sub>Bi<sub>0.16</sub>O<sub>7</sub> in Figure 1 is probably derived from the decomposition of LLZTBO due to the drastic  $C_{\text{Li}}$  difference between SnO<sub>2</sub> and LLZTBO, resulting in Li-ion loss from electrolyte to electrode. The reaction between Li ions and SnO<sub>2</sub> initiated the generation of Li<sub>2</sub>SnO<sub>3</sub>. Notably, the weight ratio of composite LLZTBO–SnO<sub>2</sub> in the work was set as 1:1, indicating that the molar ratio of LLZTBO and SnO<sub>2</sub> was about 1:5.88. Thus, the chemical reaction between LLZTBO and SnO<sub>2</sub> after cosintering at 850 °C for 5 h could be estimated as below:



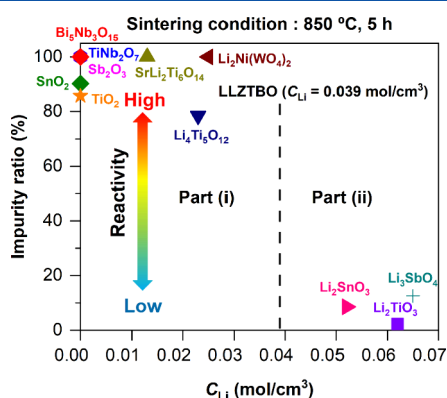
Phase identification of the TiO<sub>2</sub>/Li<sub>4</sub>Ti<sub>5</sub>O<sub>12</sub>/Li<sub>2</sub>TiO<sub>3</sub> comparative group was conducted and is recorded in Figure 2.



**Figure 2.** XRD patterns of Li<sub>4</sub>Ti<sub>5</sub>O<sub>12</sub>, Li<sub>2</sub>TiO<sub>3</sub>, LLZTBO–TiO<sub>2</sub>, LLZTBO–Li<sub>4</sub>Ti<sub>5</sub>O<sub>12</sub>, and LLZTBO–Li<sub>2</sub>TiO<sub>3</sub> pellets.

XRD results were consistent with those of  $\text{SnO}_2/\text{Li}_2\text{SnO}_3$ . Low reactivity between  $\text{Li}_2\text{TiO}_3$  in the high  $C_{\text{Li}}$  group and LLZTBO after cosintering at  $850^\circ\text{C}$  for 5 h could be concluded due to the presence of the diffraction peaks of electrolyte and anode material in the LLZTBO– $\text{Li}_2\text{TiO}_3$  composite pellets. Contrarily, no matching of active materials or LLZTBO reflects in LLZTBO– $\text{Li}_4\text{Ti}_5\text{O}_{12}$  as well as LLZTBO– $\text{TiO}_2$  in Figure 2 implies that  $\text{Li}_4\text{Ti}_5\text{O}_{12}$  or  $\text{TiO}_2$  in the low  $C_{\text{Li}}$  group completely reacted with LLZTBO after cosintering at  $850^\circ\text{C}$ . Notably, the appearance of  $\text{La}_{2.4}\text{Zr}_{1.2}\text{Ta}_{0.24}\text{Bi}_{0.16}\text{O}_7$  diffraction peak in LLZTBO– $\text{Li}_4\text{Ti}_5\text{O}_{12}$  indicated the decomposition of LLZTBO. Moreover, the appearance of various Li–La–Ti–O compounds reflected the absence of  $\text{La}_{2.4}\text{Zr}_{1.2}\text{Ta}_{0.24}\text{Bi}_{0.16}\text{O}_7$  in the LLZTBO– $\text{TiO}_2$  composite pellets, indicating the subsequent inter-reaction between intermediates and fluorite-type species. Thereafter, XRD results of  $\text{Sb}_2\text{O}_3/\text{Li}_3\text{SbO}_4$  comparative group, as well as the rest of the anode candidates in the low  $C_{\text{Li}}$  group, were conducted (Figures S1–S5). All of the  $C_{\text{Li}}$  materials reacted with LLZTBO at  $850^\circ\text{C}$ , and LLZTBO disappeared as well.

Based on the above results, the relationship between  $C_{\text{Li}}$  in the electrode materials and the reactivity with LLZTBO has been summarized in Figure 3. As can be seen, the relationship



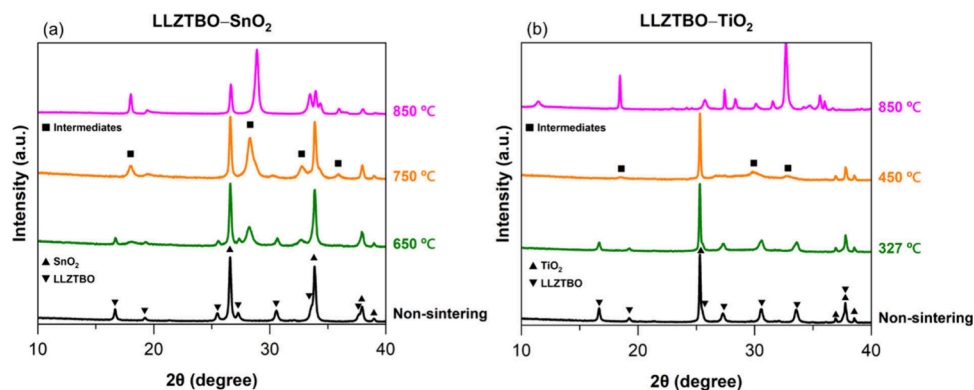
**Figure 3.** Relationship between  $C_{\text{Li}}$  in the electrode materials and the reactivity of LLZTBO.

could be divided into two parts: (i) Low  $C_{\text{Li}}$  group showing high reactivity with LLZTB, and (ii) high  $C_{\text{Li}}$  group showing low reactivity with LLZTBO. In the case of highly reactive anode candidates in part (i), the huge difference in  $C_{\text{Li}}$  between anode and LLZTB is a prerequisite of lithium diffusion from electrolyte to electrode during high-temperature

sintering, leading to drastic loss of lithium ion in LLZTBO, thus decomposing the LLZTBO crystal structure, and the subsequent chemical interaction occurred between intermediate of LLZTB and anode material. On the other hand, materials with larger  $C_{\text{Li}}$  than that of LLZTBO in part (ii) exhibit strong chemical stability against LLZTB even at  $850^\circ\text{C}$ . As the driving force of the  $C_{\text{Li}}$  difference no longer exists, LLZTBO can easily maintain its structure after sintering, leading to the successful preparation of the cosintered composite anode material.

The above results demonstrated that anode candidates in the low  $C_{\text{Li}}$  group show strong reactivity with LLZTBO. Therefore, the starting reaction temperature could be considered as an index to define the driving force of interaction between LLZTBO and anode candidates with a low  $C_{\text{Li}}$ . The range of the minimum reaction temperature ( $T_{\text{R}}$ ) could be easily characterized through XRD results and by sintering at different temperatures. Figure 4(a) and Figure 4(b) show the peak changes of LLZTBO– $\text{SnO}_2$  and LLZTBO– $\text{TiO}_2$  at different temperatures, respectively. In Figure 4(a), the diffraction peaks of LLZTBO and  $\text{SnO}_2$  remained after sintering at  $650^\circ\text{C}$ , compared to the pristine composite sample. When the temperature increased to  $750^\circ\text{C}$ , the diffraction peak of LLZTBO disappeared, whereas new peaks of intermediates could be observed. Therefore, the reaction-starting temperature between LLZTBO and  $\text{SnO}_2$  was between  $650$  and  $750^\circ\text{C}$ . Moreover, as seen in Figure 4(b), when sintering at  $327^\circ\text{C}$ , although the XRD pattern matched that of pristine composite samples, the intensity of the LLZTBO peak decreased. As the sintering temperature further increased to  $450^\circ\text{C}$ , the reaction between  $\text{TiO}_2$  and LLZTBO proceeded because of the absence of LLZTBO as well as the presence of an intermediate diffraction peak. Thus, the initial reaction temperature of composite LLZTBO– $\text{TiO}_2$  was predicted between  $327$  and  $450^\circ\text{C}$ .

Furthermore, XRD patterns of the other candidates are shown in the Supporting Information (Figures S6–S11). The range of reaction-starting temperatures of different candidates is summarized in Table 2.  $\text{Sb}_2\text{O}_3$  exhibited the strongest driving force of interfacial reaction with LLZTBO among all the candidates due to the lowest initial reaction temperature against LLZTBO. The chemical stability of  $\text{TiO}_2$ ,  $\text{Bi}_5\text{Nb}_3\text{O}_{15}$ ,  $\text{Li}_4\text{Ti}_5\text{O}_{12}$ , and  $\text{Li}_2\text{Ni}(\text{WO}_4)_2$  was in the middle class, which was stronger than that of  $\text{Sb}_2\text{O}_3$ . Notably, the interfacial reaction driving forces of  $\text{TiNb}_2\text{O}_7$ ,  $\text{SrLi}_2\text{Ti}_6\text{O}_{14}$ , and  $\text{SnO}_2$  against LLZTBO were weaker than those of the middle class,



**Figure 4.** XRD patterns of (a) LLZTBO– $\text{SnO}_2$  and (b) LLZTBO– $\text{TiO}_2$  sintering at different temperatures.

**Table 2. Range of Starting Reaction Temperature of Cosintered LLZTBO and Low  $C_{Li}$  Group Materials**

Anode materials	Li-concentration $C_{Li}$ [mol/cm <sup>3</sup> ]	Range of Min $T_R$
Sb <sub>2</sub> O <sub>3</sub>	0	253–333 °C
TiO <sub>2</sub>	0	327–450 °C
Bi <sub>5</sub> Nb <sub>3</sub> O <sub>15</sub>	0	346–450 °C
Li <sub>4</sub> Ti <sub>5</sub> O <sub>12</sub>	0.030	375–450 °C
Li <sub>2</sub> Ni(WO <sub>4</sub> ) <sub>2</sub>	0.025	388–450 °C
TiNb <sub>2</sub> O <sub>7</sub>	0	450–550 °C
SrLi <sub>2</sub> Ti <sub>6</sub> O <sub>14</sub>	0.014	550–650 °C
SnO <sub>2</sub>	0	650–750 °C

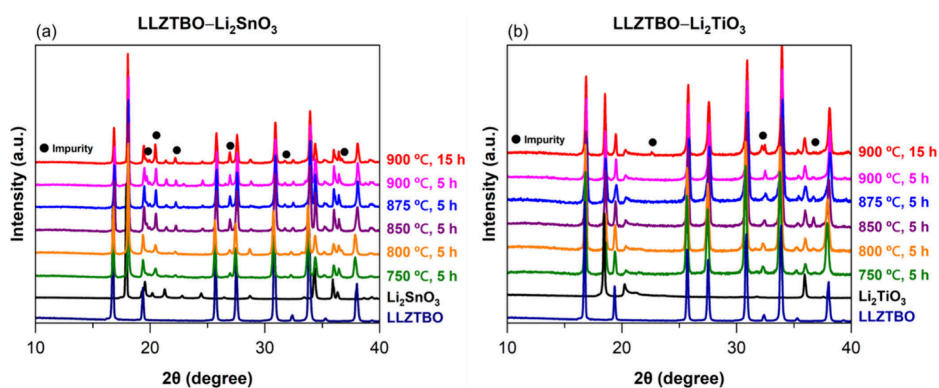
with the forces decreasing in order. Therefore, among the group of materials with low  $C_{Li}$ , no clear correlation was observed between the onset temperature of the reaction with LLZTBO and the  $C_{Li}$ . This implied that the reaction onset temperature was governed not by the reaction rate driven by differences in Li concentration (i.e., chemical potential) but, rather, by the thermodynamic factors specific to each material. These findings indicated that while  $C_{Li}$  alone could not precisely predict the ease of reaction progression between active materials and LLZTBO, it did allow for a rough classification of reactivity. Consequently, this approach proved useful for the initial screening of material systems suitable for cosintering with LLZTBO.

The high  $C_{Li}$  group, including Li<sub>2</sub>SnO<sub>3</sub>, Li<sub>2</sub>TiO<sub>3</sub>, and Li<sub>3</sub>SbO<sub>4</sub>, showed strong chemical stability against LLZTBO cosintering at 850 °C, which could be considered as promising cosintered type anode candidates of garnet-type solid-state electrolyte. To understand the detailed behavior during the sintering process, we investigated the sintering temperature dependence of the reactivity with LLZTBO. The XRD patterns of LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> and LLZTBO–Li<sub>2</sub>TiO<sub>3</sub> after sintering at various temperatures are shown in Figure 5(a,b). For LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> composite samples, no obvious peak change could be observed through the XRD patterns, suggesting that Li<sub>2</sub>SnO<sub>3</sub> can be cosintered with LLZTBO, leading to strong chemical stability. Additionally, in the case of the composite LLZTBO–Li<sub>2</sub>TiO<sub>3</sub>, no obvious peak difference could be observed when sintering from 750 to 900 °C for 5 h. An additional impurity peak appeared when the sintering time was extended from 5 to 15 h at 900 °C; these unknown species might contribute to increased interdiffusion between the anode and electrolyte, as well as the side reaction occurring at the interface, as described in detail later. The same tendency was

also confirmed from the results of LLZTBO–Li<sub>3</sub>SbO<sub>4</sub> shown in Figure S12.

**3.2. Sintering Behavior and Characterization of Composite Pellets.** The relative density of the cosintered pellet is significant for designing the all-solid-state battery. Low relative density leads to high electrical resistance related to electronic and ionic conduction, resulting in poor battery performance. Therefore, relative densities of composite LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> and LLZTBO–Li<sub>2</sub>TiO<sub>3</sub> pellets as a function of the sintering temperature have been measured and shown in Figure 6(a) and (b), respectively. As seen in Figure 6, the relative densities of both LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> and LLZTBO–Li<sub>2</sub>TiO<sub>3</sub> pellets increased with an increase in the sintering temperature. When further extending the sintering time from 5 to 15 h at 900 °C, the relative densities of LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> and LLZTBO–Li<sub>2</sub>TiO<sub>3</sub> could achieve as high as 89% and 95%, respectively. In addition, the relative density of LLZTBO–Li<sub>3</sub>SbO<sub>4</sub> is shown in Figure S13. These results demonstrated high potential for high  $C_{Li}$  materials as the anode materials suitable for cosintering and densification with LLZTBO.

To evaluate the interdiffusion of composite pellets after cosintering, lattice parameter  $a$  of cubic LLZTBO ( $a = b = c$ ) and standard data were analyzed by Rietveld refinement in Figure 7. The results of LLZTBO–Li<sub>3</sub>SbO<sub>4</sub> are shown in Figure S14. ICSD No. 22957 (crystal structure: cubic Li<sub>6.5</sub>La<sub>3</sub>Zr<sub>1.5</sub>Ta<sub>0.5</sub>O<sub>12</sub>, space group:  $Ia3d$ ) was used as the initial model. As seen in Figure 7, compared with the cubic LLZTBO, a larger lattice parameter  $a$  of LLZTBO after ball-milling could be observed, which originated from the proton exchange that occurred, resulting in the formation of H-substituted LLZTBO. Thereafter, this H-substituted LLZTBO gradually reverted to its original LLZ structure as the sintering temperature increased. It is noted that the lattice parameter after sintering at high temperature strongly depends on the kinds of cosintered electrode materials. When LLZTB is sintered alone or cosintered with Li<sub>2</sub>SnO<sub>3</sub>, no significant change in lattice parameter is observed. However, cosintering with Li<sub>2</sub>TiO<sub>3</sub> and Li<sub>3</sub>SbO<sub>4</sub> shows a tendency for the lattice parameter to decrease. Here, the ionic radii of the elements contained in each electrode material follow the order: Sb<sup>5+</sup> (0.6 Å) < Ti<sup>4+</sup> (0.605 Å) < Sn<sup>4+</sup> (0.69 Å) < Zr<sup>4+</sup> (0.72 Å).<sup>59</sup> Based on the TEM observations discussed later, these elements are likely to undergo mutual diffusion with Zr and become incorporated into the LLZ structure as a solid solution. Therefore, the decrease in the lattice parameter observed during high-temperature sintering, which depends on the type

**Figure 5.** Sintering temperature dependence of (a) LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> and (b) LLZTBO–Li<sub>2</sub>TiO<sub>3</sub>.

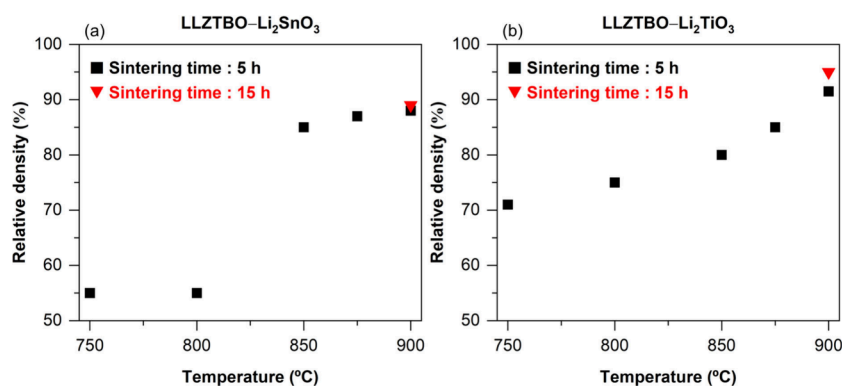


Figure 6. Relative densities of (a) LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> and (b) LLZTBO–Li<sub>2</sub>TiO<sub>3</sub> as a function of the sintering temperature.

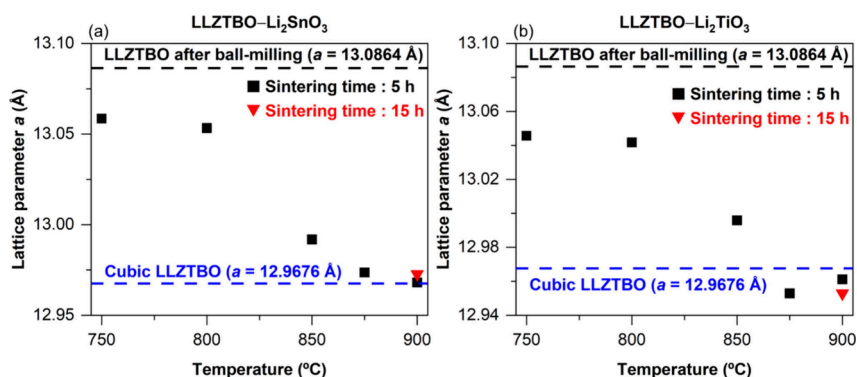


Figure 7. Lattice parameter *a* of LLZTBO in (a) LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> and (b) LLZTBO–Li<sub>2</sub>TiO<sub>3</sub> as a function of the sintering temperature.

of electrode material, is considered to result from the substitution of smaller ions from the electrode into the LLZ lattice in place of Zr.

Specifically, to reveal the interdiffusion as well as the side reaction occurred at the interface, the enlarged TEM images and element distribution of LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> sintering at 900 °C for 15 h were conducted and shown in Figure 8. The overall TEM image and element mappings of LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> are shown in Figure S15. The overlap within the Sn-rich parts, the Zr-rich parts, and the La-rich parts showed three different areas: A, B, and C. Mass ratios of each element in these three areas using EDS are summarized in Table 3. According to the results of quantitative analysis, Area A was considered to contain Li<sub>2</sub>SnO<sub>3</sub> with a small amount of Zr diffused from LLZTBO. The Sn–Zr–O contained substance in Area B suggested the impurity contributed by the side reaction at the LLZTBO and Li<sub>2</sub>SnO<sub>3</sub> interface. Area C matched the La-rich parts, which reflected the LLZTBO with Sn diffused into the Zr sites. TEM results showed that interdiffusion in the composite LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> pellet was critical. The generation of such impurities might significantly increase the interfacial resistance, leading to the degradation of battery performance.<sup>60</sup> Therefore, interdiffusion between the anode and LLZTBO should be a priority to consider in the design of the battery. Element substitution into LLZ could be considered a possible approach to achieve interdiffusion suppression.

**3.3. Electrode Performance for Composite Anode Pellets.** Finally, to reveal the electrode property for high C<sub>Li</sub> materials cosintered with LLZTBO, charge–discharge tests of Li | 1 M LiPF<sub>6</sub> | LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> and Li | 1 M LiPF<sub>6</sub> | LLZTBO–Li<sub>2</sub>TiO<sub>3</sub> have been carried out at room temperature

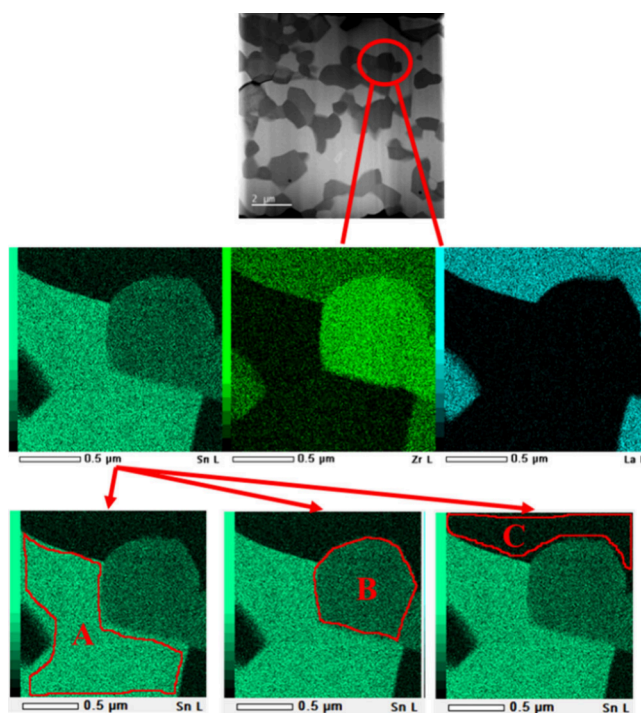


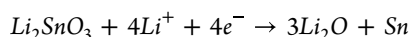
Figure 8. TEM images and elemental mappings of the Sn-rich, Zr-rich, and La-rich parts of LLZTBO–Li<sub>2</sub>SnO<sub>3</sub> sintering at 900 °C for 15 h.

and shown in Figure 9. As seen in Figure 9(a), a typical reversible charge–discharge curve of Li<sub>2</sub>SnO<sub>3</sub> successfully appeared at a constant current density of 134 μA/cm<sup>2</sup> (0.01C).

Table 3. Mass Ratio of Elements in Different Parts

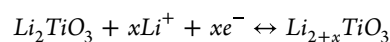
Element	Mass ratio [%]		
	A	B	C
O	26.96	25.32	16.59
Zr	1.78	32.25	12.35
Sn	70.17	40.38	8.12
La	0.28	1.03	51.63
Ta	0.42	0.56	5.07
Bi	0.38	0.45	6.23
Total	100	100	100

A huge drop of the potential at initial discharge (Cycle 1) indicated a significant polarization of the anode due to the poor electrical conductivity of  $\text{Li}_2\text{SnO}_3$  ( $\sim 10^{-9}$  S/cm) as reported,<sup>57</sup> meanwhile, the smooth discharge curve from second cycle was attributed to the formation of Sn-metal,<sup>61</sup> resulting in significant electrical conductivity improvement of anode. Surprisingly, the discharge capacity in the first cycle was around 600 mAh/g. Nevertheless, nearly 250 mAh/g of irreversible discharge capacity appeared at the first delithiation process (the Coulombic efficiency: 63%), which was coming from the formation of the solid electrolyte interface (SEI) and huge volume expansion of  $\text{Li}_2\text{SnO}_3$ . However, Coulombic efficiency at the second cycle was as high as 92% with nearly 600 mAh/g of reversible capacity, which was due to a significant enhancement of electrical conductivity related to the formation of Sn metal.<sup>61</sup> As a reference, the battery performance of the  $\text{Li}_2\text{SnO}_3$  (via SSR) electrode, composed with acetylene black and PVDF binder, was reported to achieve nearly 400 mAh/g reversible capacity at a current of 60 mA/g, with a capacity fading rate of about 0.4% per cycle.<sup>62</sup> The chemical reaction as well as the lithiation/delithiation process of the  $\text{Li}_2\text{SnO}_3$  electrode during charge–discharge were written as<sup>62</sup>



Despite the successful proof of composite LLZTBO– $\text{Li}_2\text{SnO}_3$  anode used for a liquid electrolyte, the electrode property of LLZTBO– $\text{Li}_2\text{TiO}_3$  was at a low level, compared to the theoretical capacity of  $\text{Li}_2\text{TiO}_3$  (229 mAh/g).<sup>63</sup> As a reference, the  $\text{Li}_2\text{TiO}_3$  (via SSR) electrode, composed with acetylene black and binder, was reported to achieve nearly 150 mAh/g specific capacity at a current of 100 mA/g, which still exhibits a specific capacity of about 121 mAh/g after 500

cycles.<sup>64</sup>  $\text{Li}_2\text{TiO}_3$  has been reported as electrochemically inert, and the electrode reaction can be described as below:<sup>64,65</sup>



Such mechanisms indicated that there was no Ti-metal product involved during the insertion/extraction of the Li ion. The same tendency could be observed in LLZTBO– $\text{Li}_3\text{SbO}_4$  composite pellets (Figure S16). Additionally, the battery performance of the  $\text{Li}_3\text{SbO}_4$  electrode, composed with acetylene black and binder, was reported to exhibit a reversible capacity of 81 mAh/g at a current density of 0.05 mA/cm<sup>2</sup> (C/5) and remain unchanged with cycling (after 100 cycles).<sup>66</sup> Contrarily, Sn-metal formation during the charge–discharge test in the LLZTBO– $\text{Li}_2\text{SnO}_3$  pellet significantly increases the electronic pathway, resulting in a large discharge capacity and good battery performance. Therefore, it could be speculated that the electronic pathway is limited in LLZTBO– $\text{Li}_2\text{TiO}_3$  due to the poor electrical properties of  $\text{Li}_2\text{TiO}_3$ . This results in intercalation and extraction of Li-ion occurring only on the current collector side, leading to poor battery performance. To suppress this, introducing an electrochemically active additive with strong chemical stability against LLZ and anode material into the composite pellet may significantly increase the electronic pathway, resulting in good battery performance.

#### 4. CONCLUSIONS

In this study, we have provided a favorable approach for screening anode candidates applicable to cosintered-type LLZ-based all-solid-state lithium batteries (ASSLBs). Herein, the relationship between lithium concentration ( $C_{\text{Li}}$ ) in the electrode materials and the reactivity of LLZTB has been investigated. The interfacial reaction of cosintered LLZ/Anode at elevated temperature is predictable: high  $C_{\text{Li}}$  materials (larger than that of LLZ) achieve interaction suppression attributed to the absence of a Li-diffusion driving force, whereas electrodes with lower  $C_{\text{Li}}$  show weak chemical stability against LLZ due to the occurrence of Li loss in LLZ. In the case of high  $C_{\text{Li}}$  materials, interdiffusion and side reactions at the interface of the composite LLZ/Anode should be carefully considered. Interdiffusion between the electrolyte and electrode leads to a decrease in the number of active materials. Meanwhile, the generation of impurities may drastically reduce the interfacial resistance, resulting in a poor battery performance. The electrode performance of the cosintered anode using a liquid electrolyte-based half-cell has been investigated. A typical reversible charge–discharge curve of the LLZTBO–

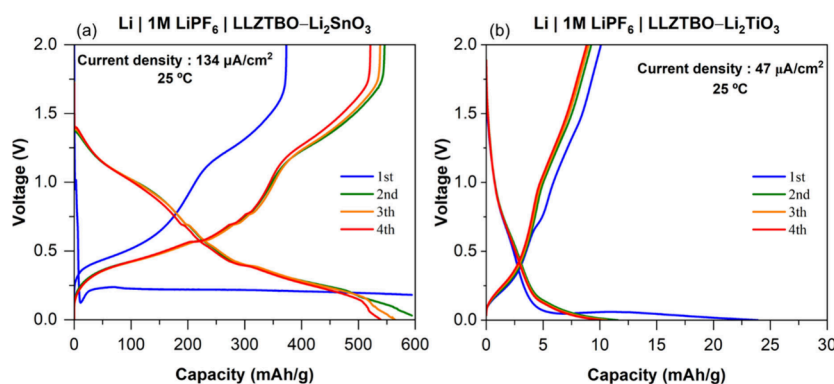


Figure 9. Charge–discharge curves of (a) Li | 1 M LiPF<sub>6</sub> | LLZTBO– $\text{Li}_2\text{SnO}_3$  and (b) Li | 1 M LiPF<sub>6</sub> | LLZTBO– $\text{Li}_2\text{TiO}_3$  at room temperature.

Li<sub>2</sub>SnO<sub>3</sub>-based half-cell could be successfully observed, and a reversible capacity of 600 mAh/g with 92% of Coulombic efficiency was achieved. These results demonstrate the effectiveness of the C<sub>Li</sub>-based materials screening, and we believe that the proposed method can accelerate the development of cosintered ASSLBs based on various electrolytes.

## ■ ASSOCIATED CONTENT

### SI Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acsaem.5c02930>.

Synthesis information on anode candidates; XRD patterns of composite materials; sintering dependence, relative densities, lattice parameter, and charge–discharge curves of LLZTBO–Li<sub>3</sub>SbO<sub>4</sub> composite disk (PDF)

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### Notes

The authors declare no competing financial interest.

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