

A NOVEL APPROACH FOR SINTERING $\text{Nd}_2\text{Fe}_{14}\text{B}$ -, SmCo_5 - AND $\text{Sm}_2\text{Co}_{17}$ -BASED MAGNETS BY THE HDDR PROCESS

Ihor I. Bulyk^{a,b,d,*}, RenHui Liu^{a,b}, HePing Zhu^a, SuJuan Wang^a, MuNan Yang^{a,b,c},
Ihor V. Borukh^d, Oleksandr P. Kononiuk^d

^a Jiangxi Province Key Laboratory of Magnetic Metallic Materials and Devices, Jiangxi University of Science and Technology, Ganzhou, 341000, PR China

^b National Rare Earth Functional Materials Innovation Center, Ganzhou 341000, China

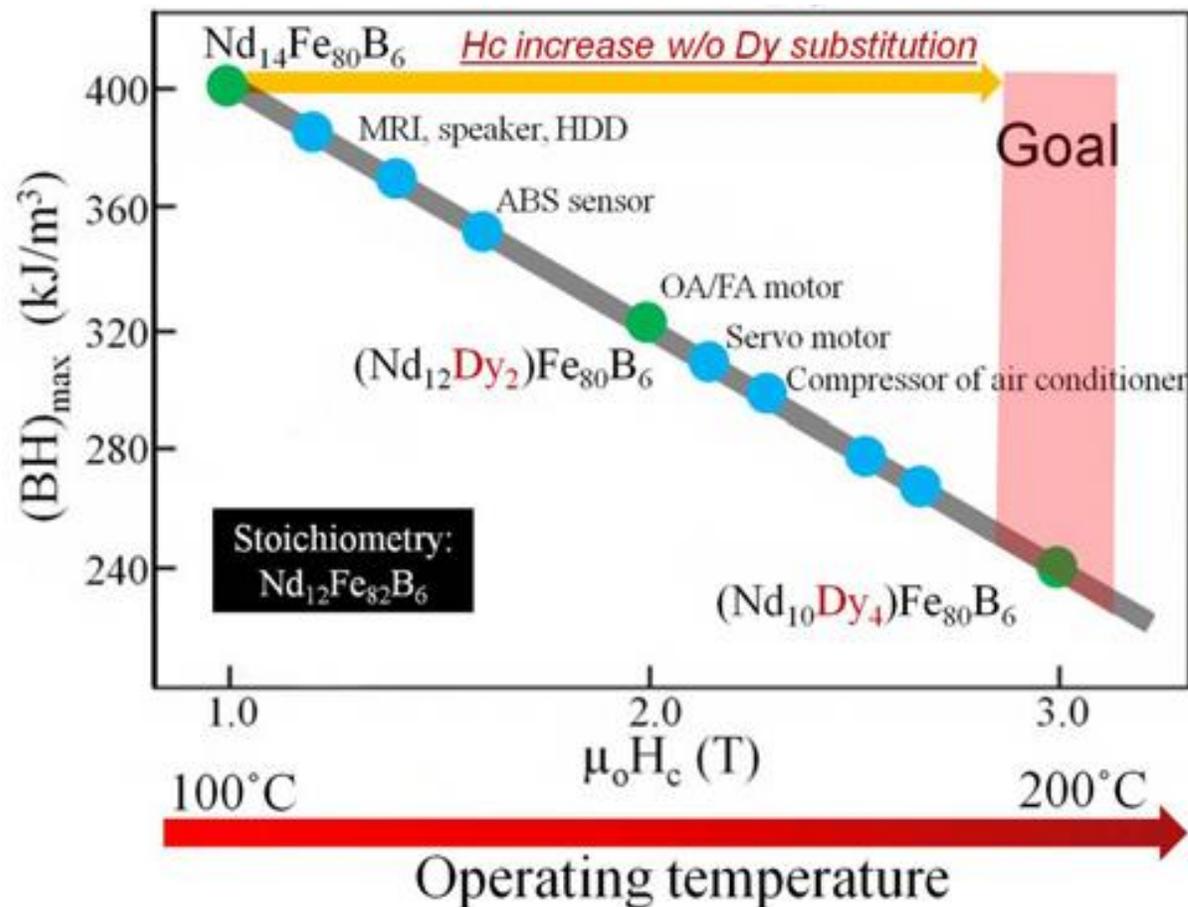
^c Ganjiang Innovation Academy, Chinese Academy of Science, Ganzhou 341000, China

^d Karpenko Physico-Mechanical Institute of National Academy of Sciences of Ukraine, Lviv, 79060, Ukraine

* bulyk@jxust.edu.cn, speaker

Requirements for Magnetic materials

For wind turbines and electric vehicles

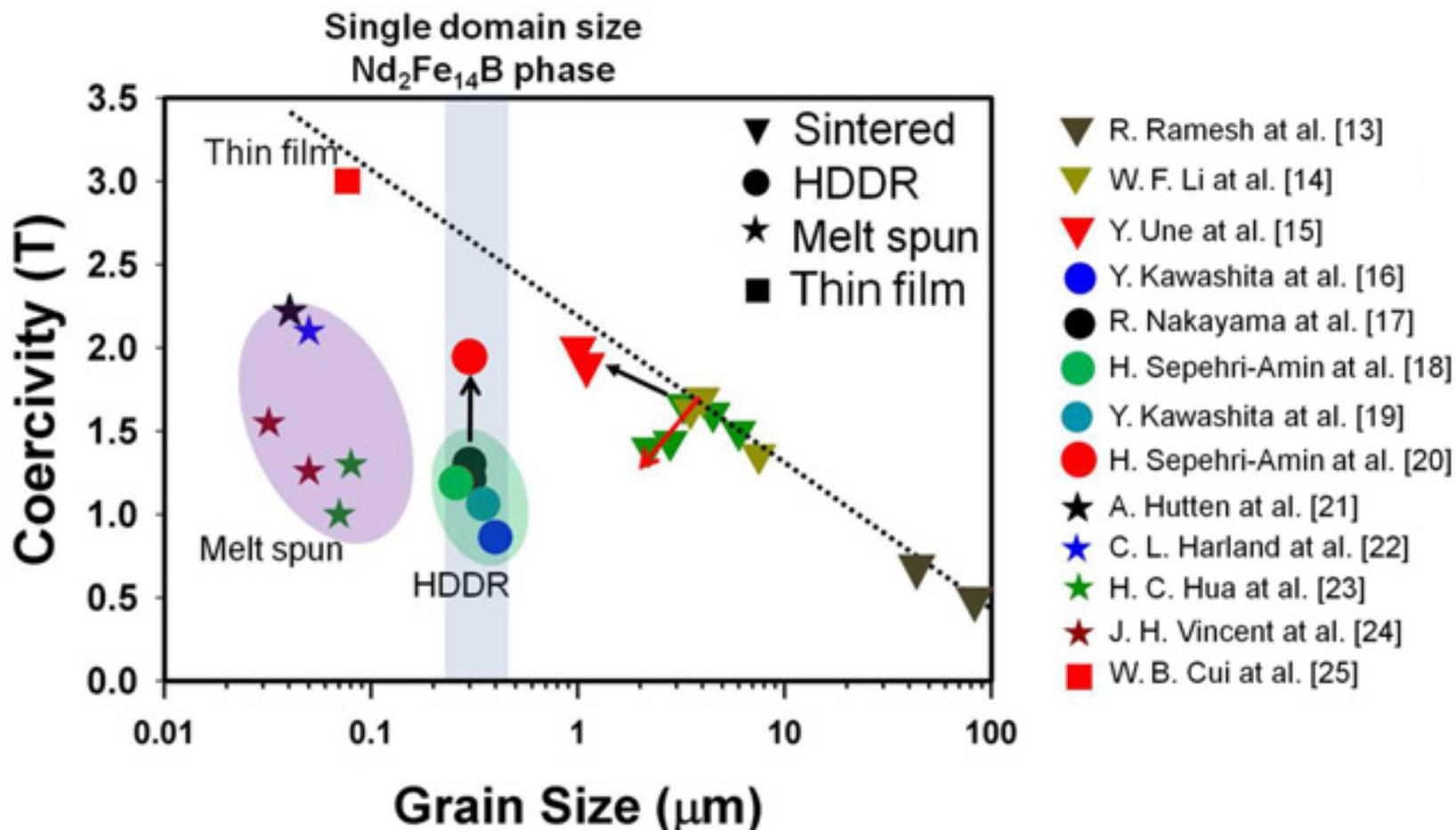


The operating temperature of the traction motors for (hybrid) electric vehicles is approximately 200 C.

Therefore, **permanent magnets suitable for use in traction motors and wind power generators must have a high coercivity of around 3 T at room temperature.**

Requirements for Magnetic materials

For wind turbines and electric vehicles



the coercivity increases as the grain size decreases

We view the HDDR process as a promising method for refining the microstructure of the R-TM ferromagnetic materials type materials, particularly R-Fe-B and Sm-Co.



R-TM ferromagnetic materials with fine microstructure

How can we produce **the bulk R-TM ferromagnetic materials** with fine microstructures?
Through the HDDR process.

SINTERING:

it occurs through **the diffusion** of material components

1. The HDDR process involves phase transformations through **diffusion** \Rightarrow the **diffusion rate** of all alloy components **increases**.

Ya.E. Geguzin, *Physics of Sintering* [in Russian], Nauka, Moscow, (1984), p. 311.

V.V. Skorokhod and S.M. Solonin, *Physical and Metallurgical Fundamentals of Powder Sintering* [in Russian], Metallurgiya, Moscow (1984), p. 159.

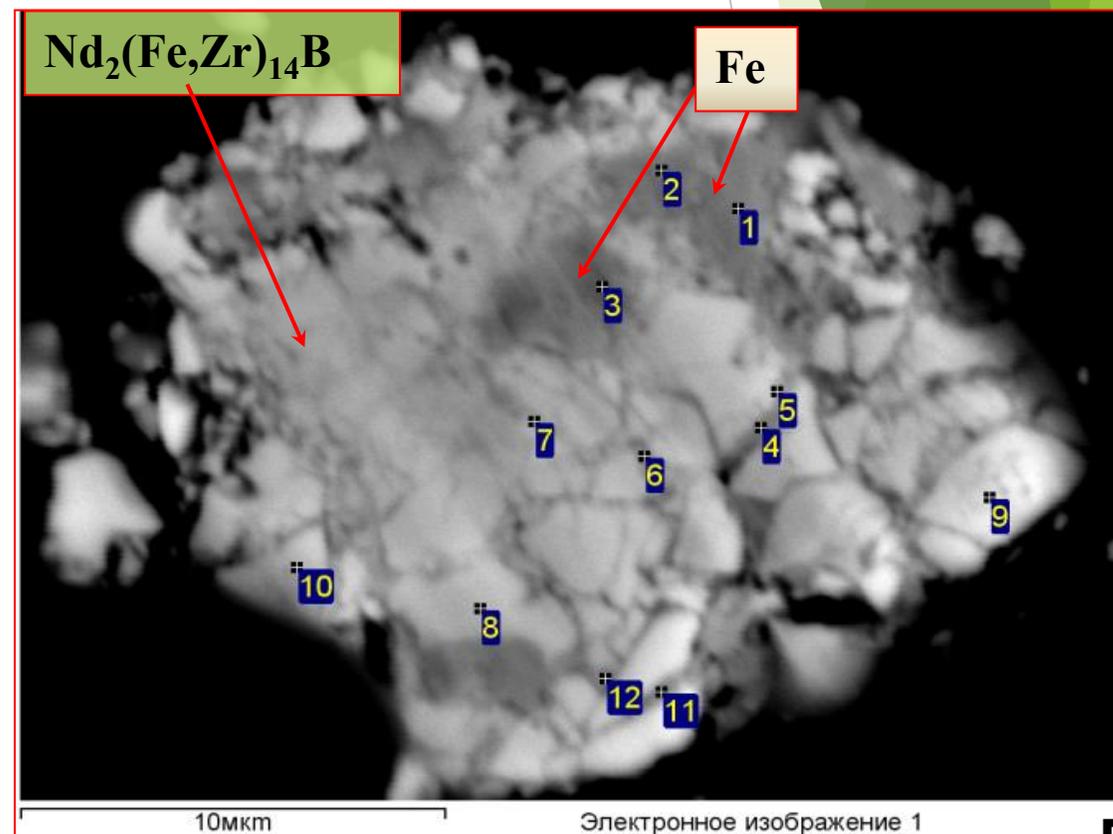
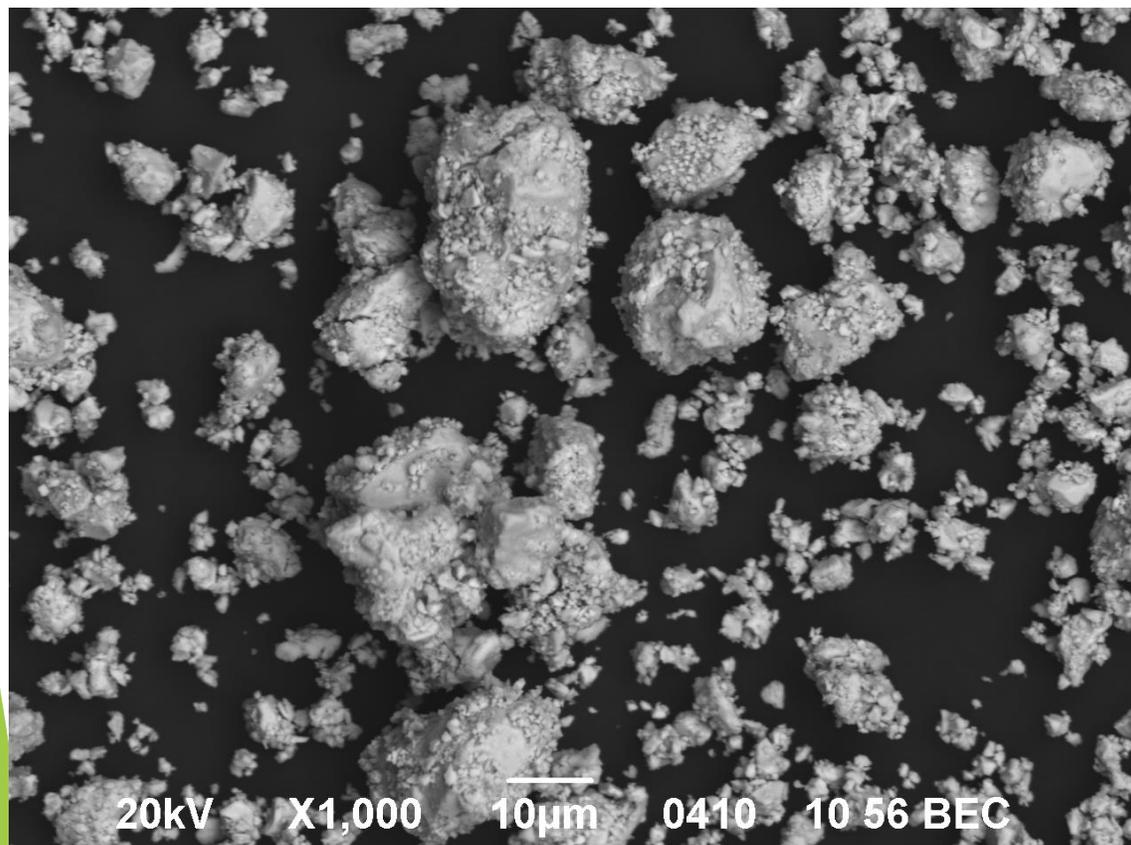
2. During HDDR, **hydrogen** is present in the alloy as a **solid solution** \Rightarrow The **diffusion rate** of all alloy components is **higher** than that of an alloy without a hydrogen solid solution.

V.I. Pokhmurskii and V.V. Fedorov, *Effect of Hydrogen on Diffusion Processes in Metals* [in Ukrainian], FMI NANU, Lviv (1998), p. 206.

The morphology and microstructure of the coarse particles of the $Nd_{11.7}Fe_{81.1}Zr_{1.2}B_6$ alloy milled in hydrogen.

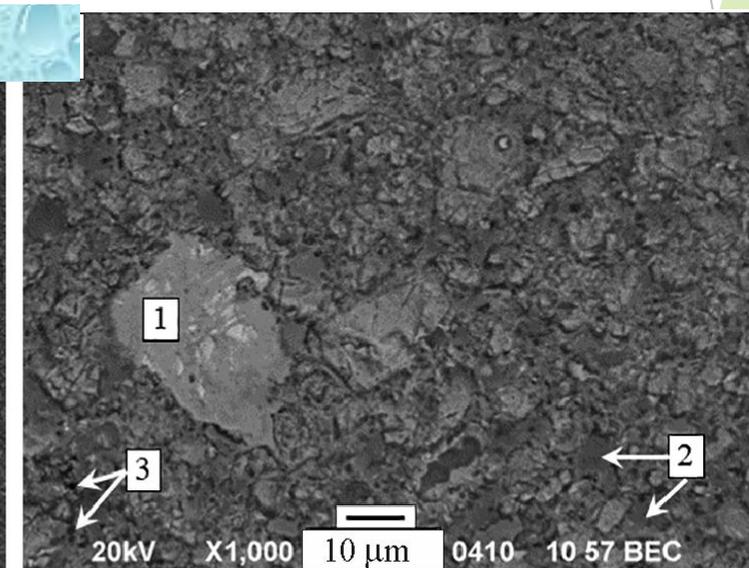
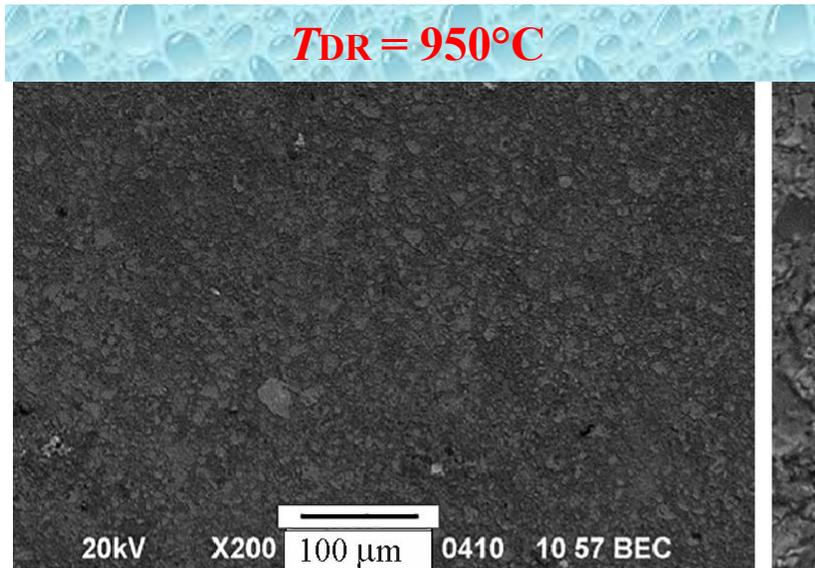
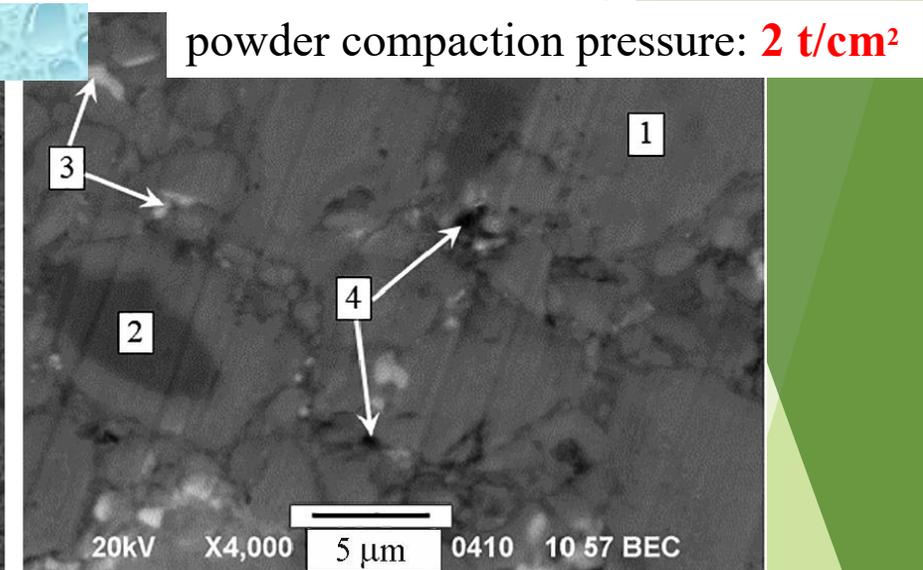
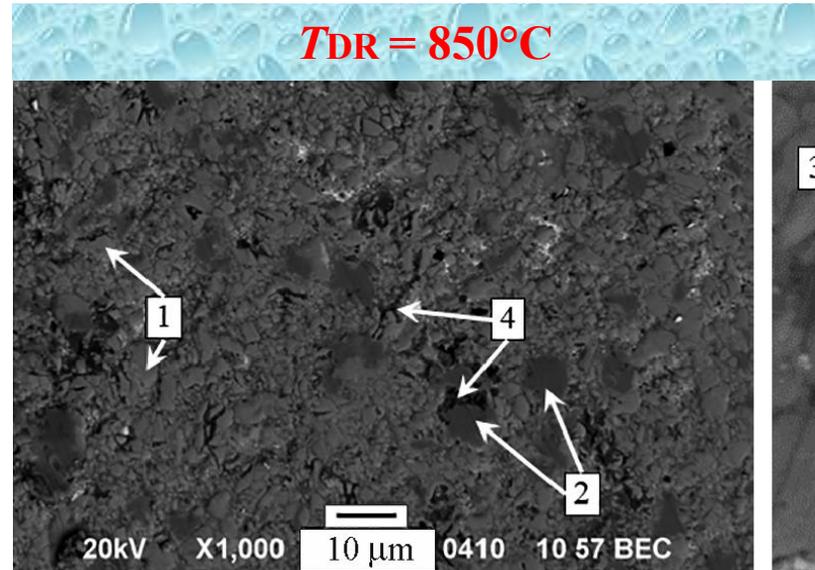
Milling terms: $v=200$ rpm, $\tau=1$ h

Particle size: from 2-3 to 10-30 microns



The microstructure of the sintered through the HDDR process
Nd_{11.7}Fe_{81.1}Zr_{1.2}B₆ alloy

- 1) Nd₂(Fe, Zr)₁₄B phase;
- 2) α -Fe-based solid solution;
- 3) Nd-rich phase;
- 4) pores



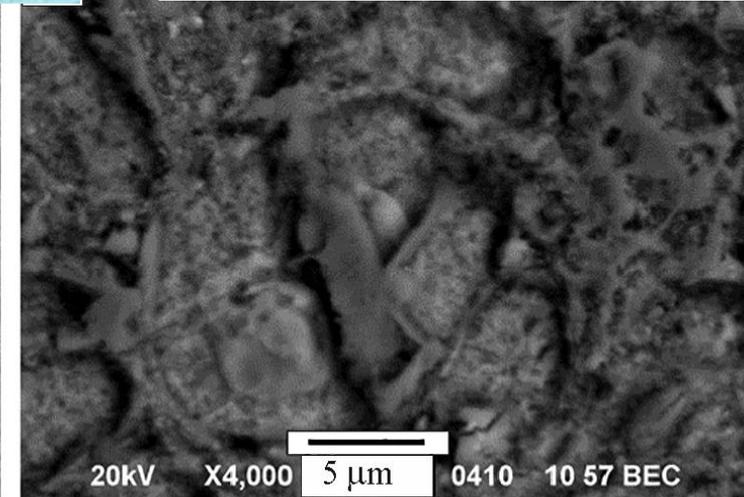
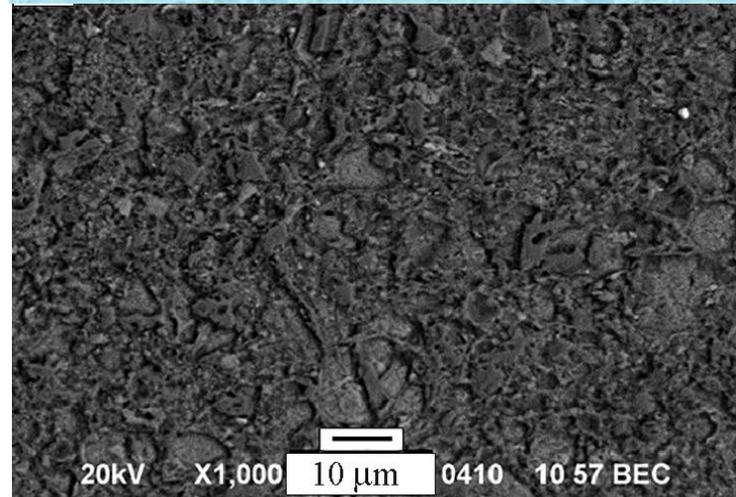
- 1) Nd₂(Fe, Zr)₁₄B phase;
- 2) α -Fe-based solid solution;
- 3) pores

Preliminary Results of Sintering $R_2Fe_{14}B$ Magnetic Materials Using the HDDR Process

The microstructure of the sintered through the HDDR process
Nd_{11.7}Fe_{81.1}Zr_{1.2}B₆ alloy

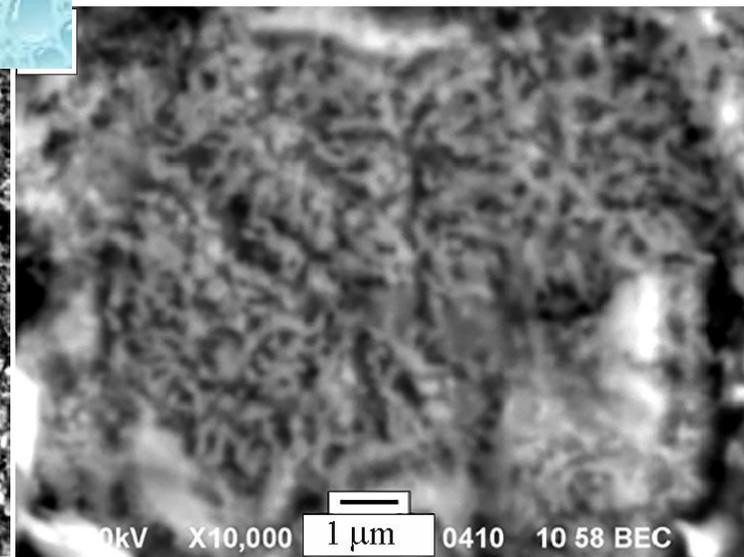
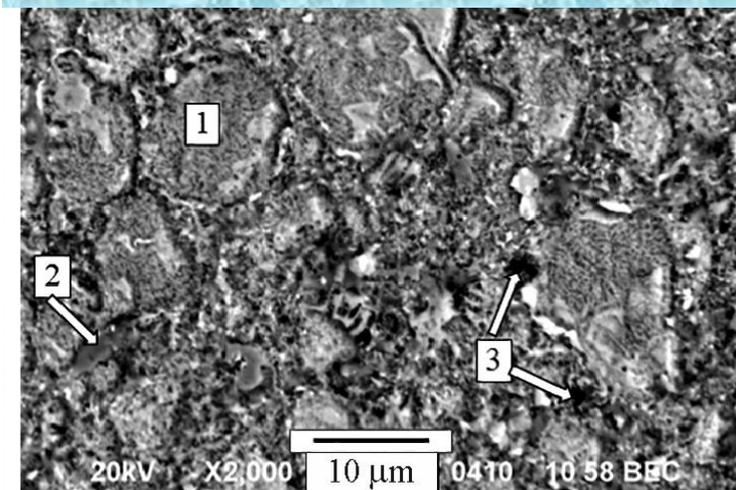
$T_{DR} = 850^\circ\text{C}$

powder compaction pressure: **5 t/cm²**



$T_{DR} = 950^\circ\text{C}$

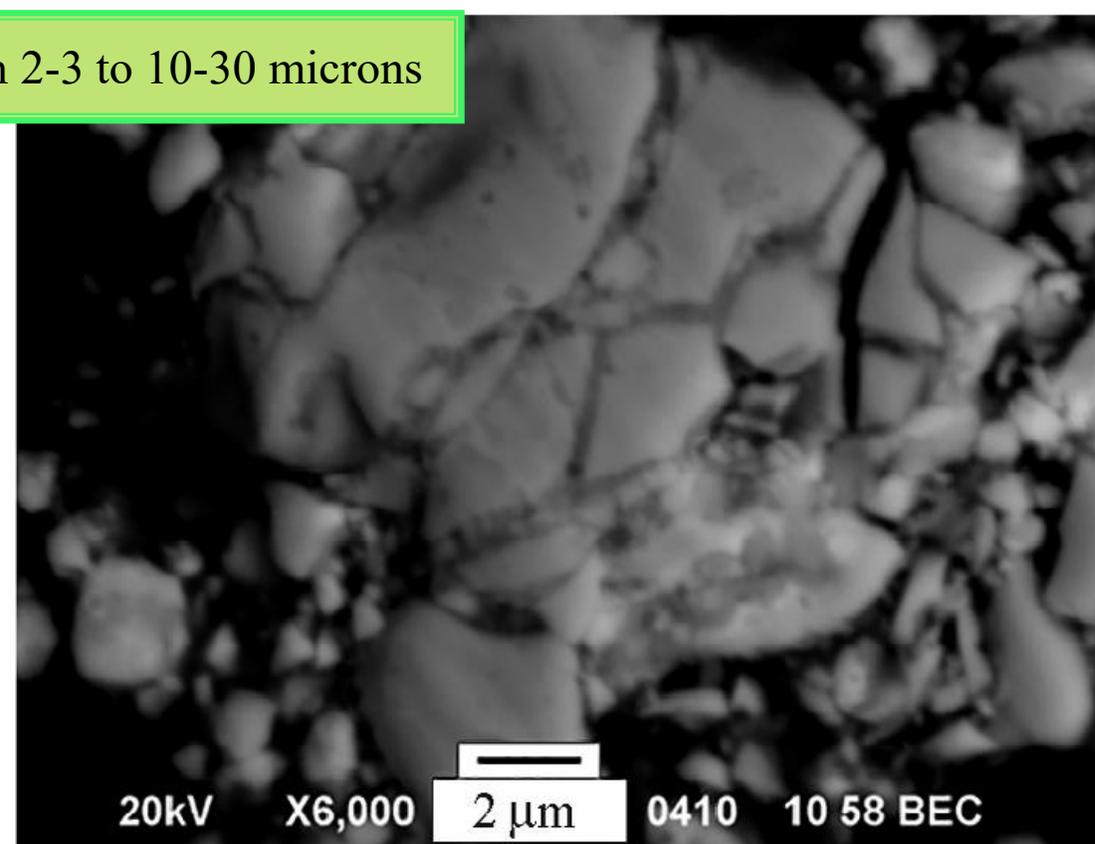
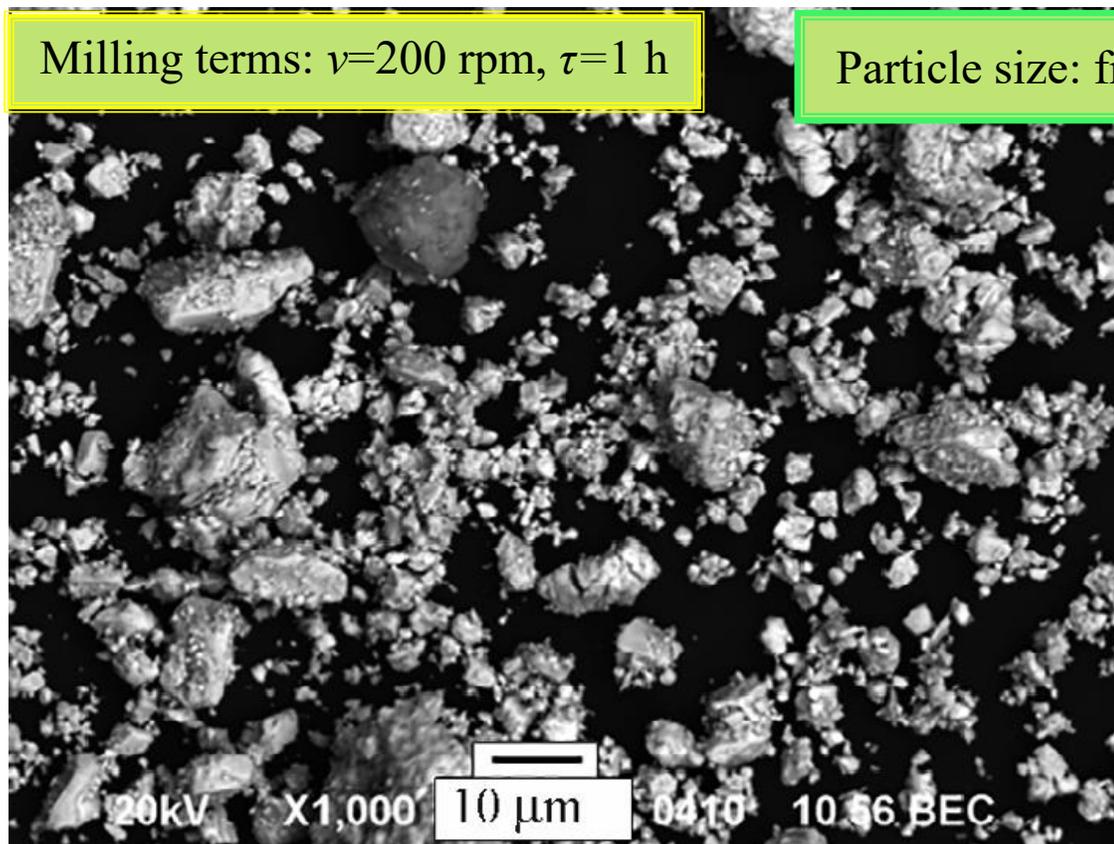
- 1) Nd₂(Fe, Zr)₁₄B phase;
- 2) α-Fe-based solid solution;
- 3) pores



The morphology and microstructure of the coarse particles of the $Nd_{16}Fe_{73.9}Zr_{2.1}B_8$ alloy milled in hydrogen

Milling terms: $v=200$ rpm, $\tau=1$ h

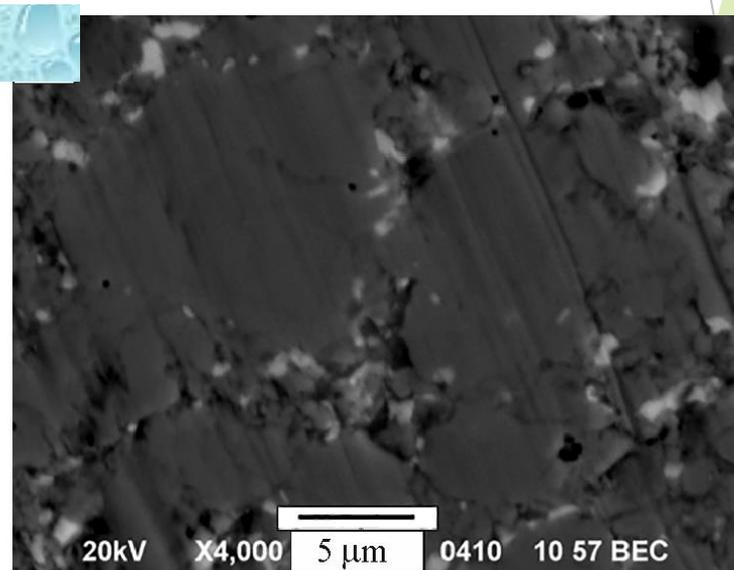
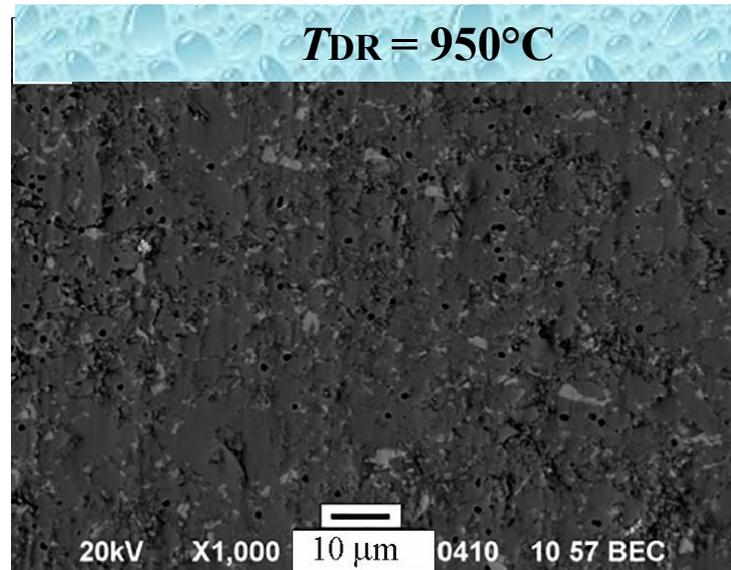
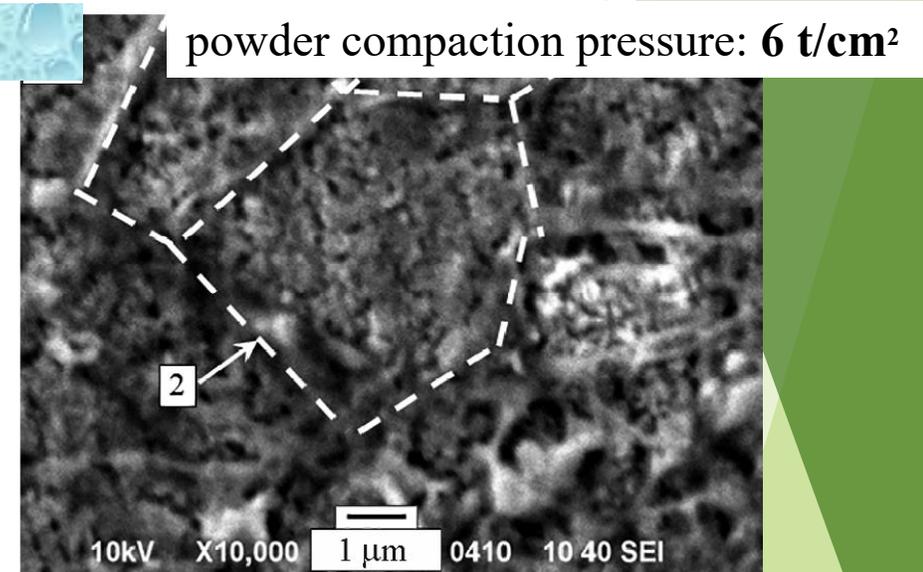
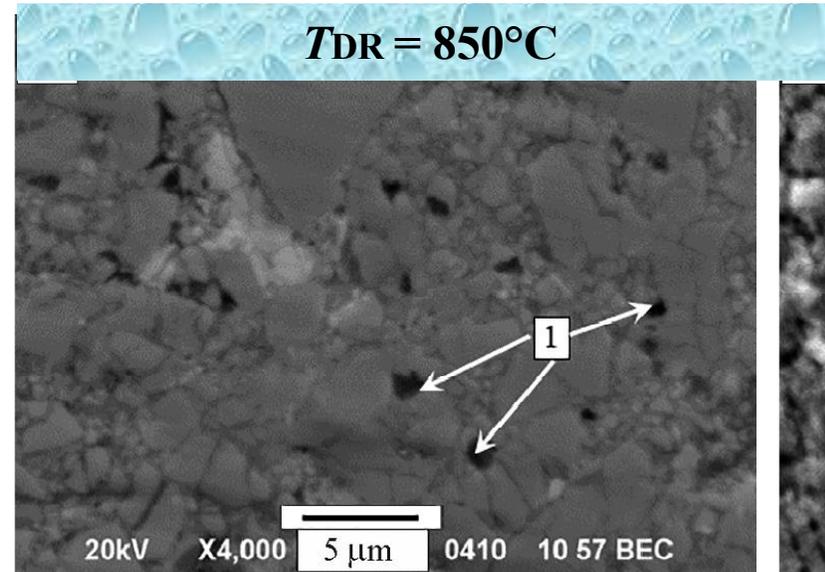
Particle size: from 2-3 to 10-30 microns



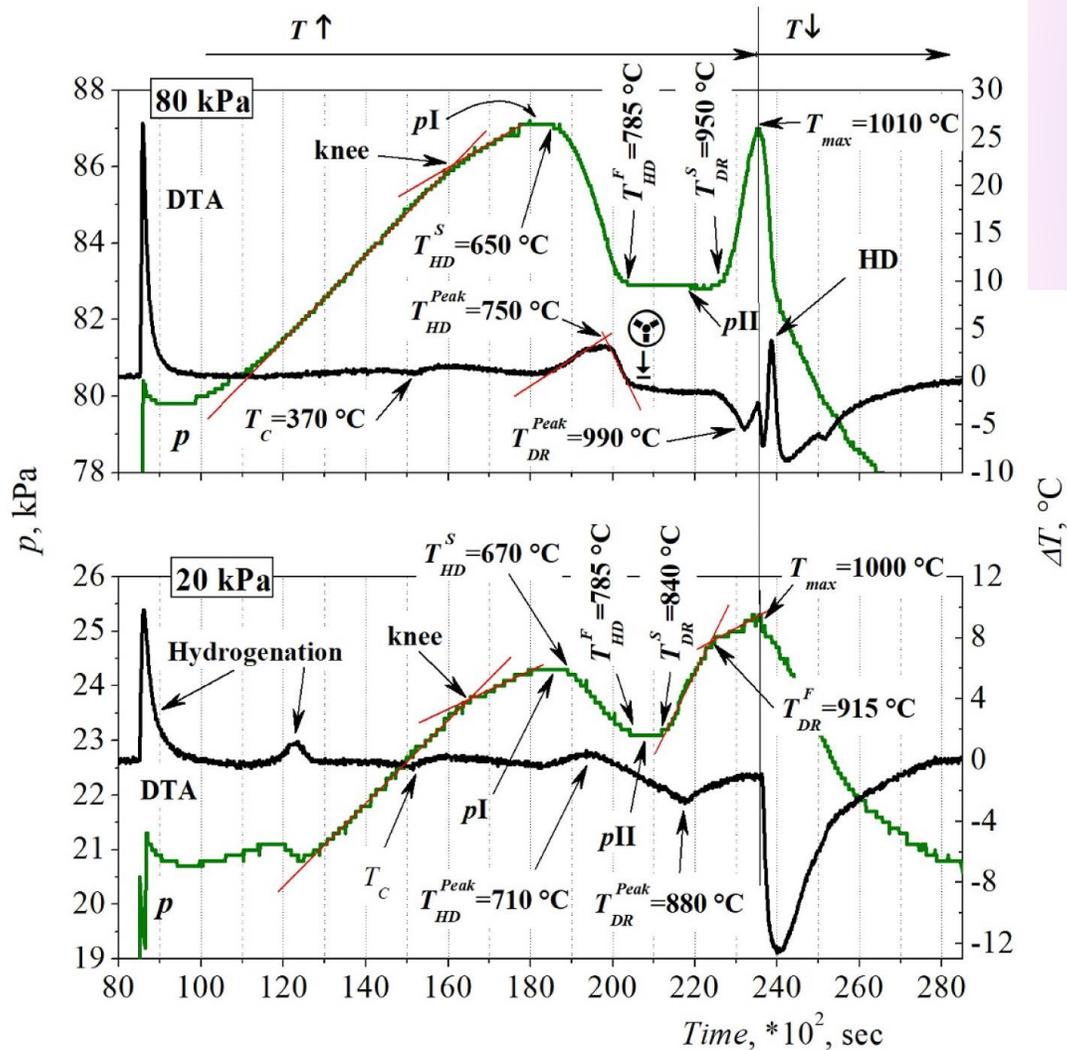
Preliminary Results of Sintering $R_2Fe_{14}B$ Magnetic Materials Using the HDDR Process

The microstructure of the sintered through the HDDR process the $Nd_{16}Fe_{73.9}Zr_{2.1}B_8$ alloy

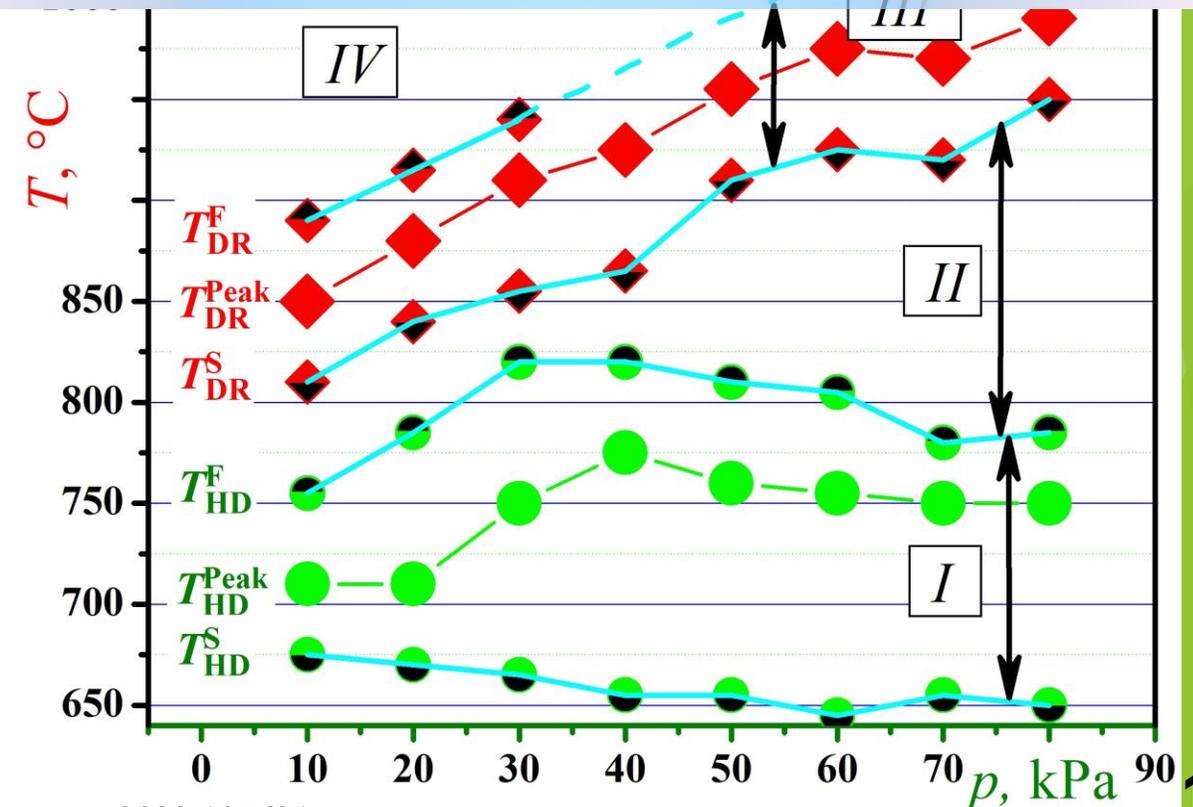
unetched section, 1) pores;
etched section, 2) boundaries between sintered particles



Sintering $R_2Fe_{14}B$ magnetic materials using the HDDR process:

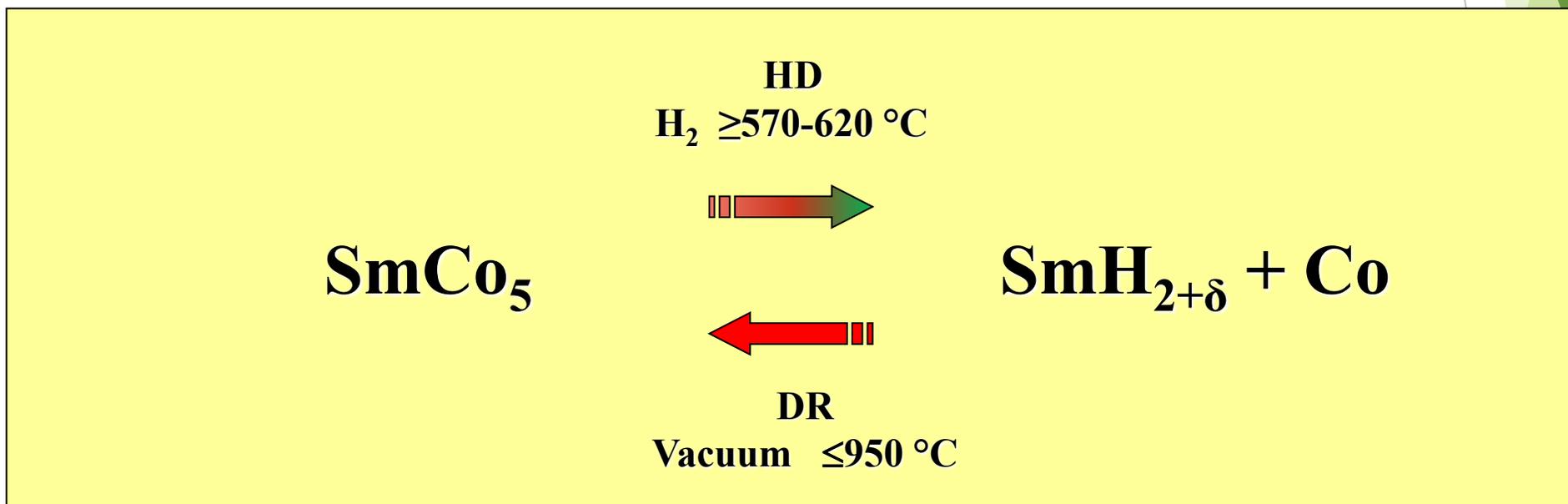


Next step:
Preparing a Pressure – Phase Composition – Temperature diagram to use as a basis for choosing HDDR parameters



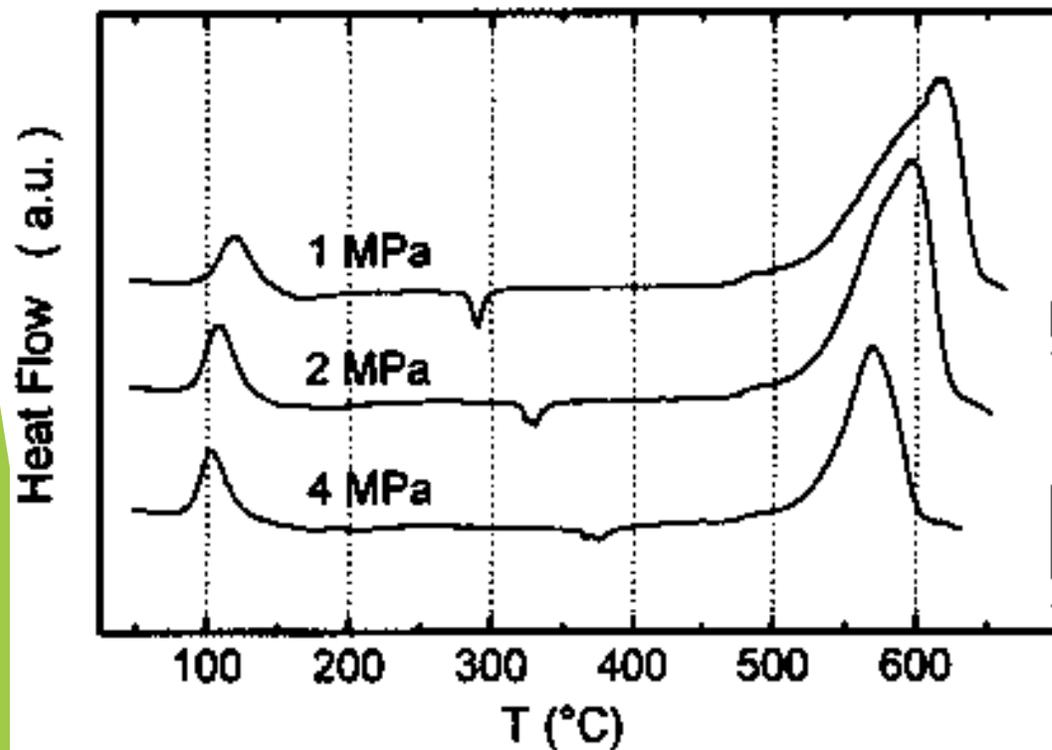
HDDR PROCESS IN SmCo_5 MATERIALS

LITERATURE DATA ABOUT HDDR IN SmCo_5 ALLOYS

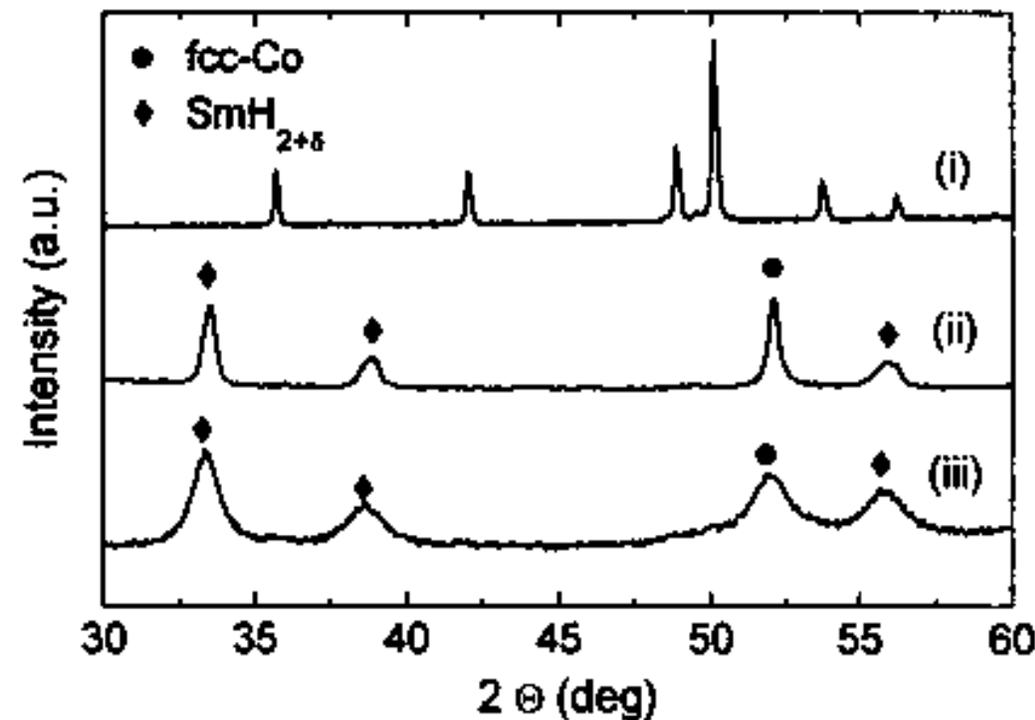


HDDR PROCESS IN SmCo_5 MATERIALS

DSC curves for SmCo_5 under different hydrogen pressures



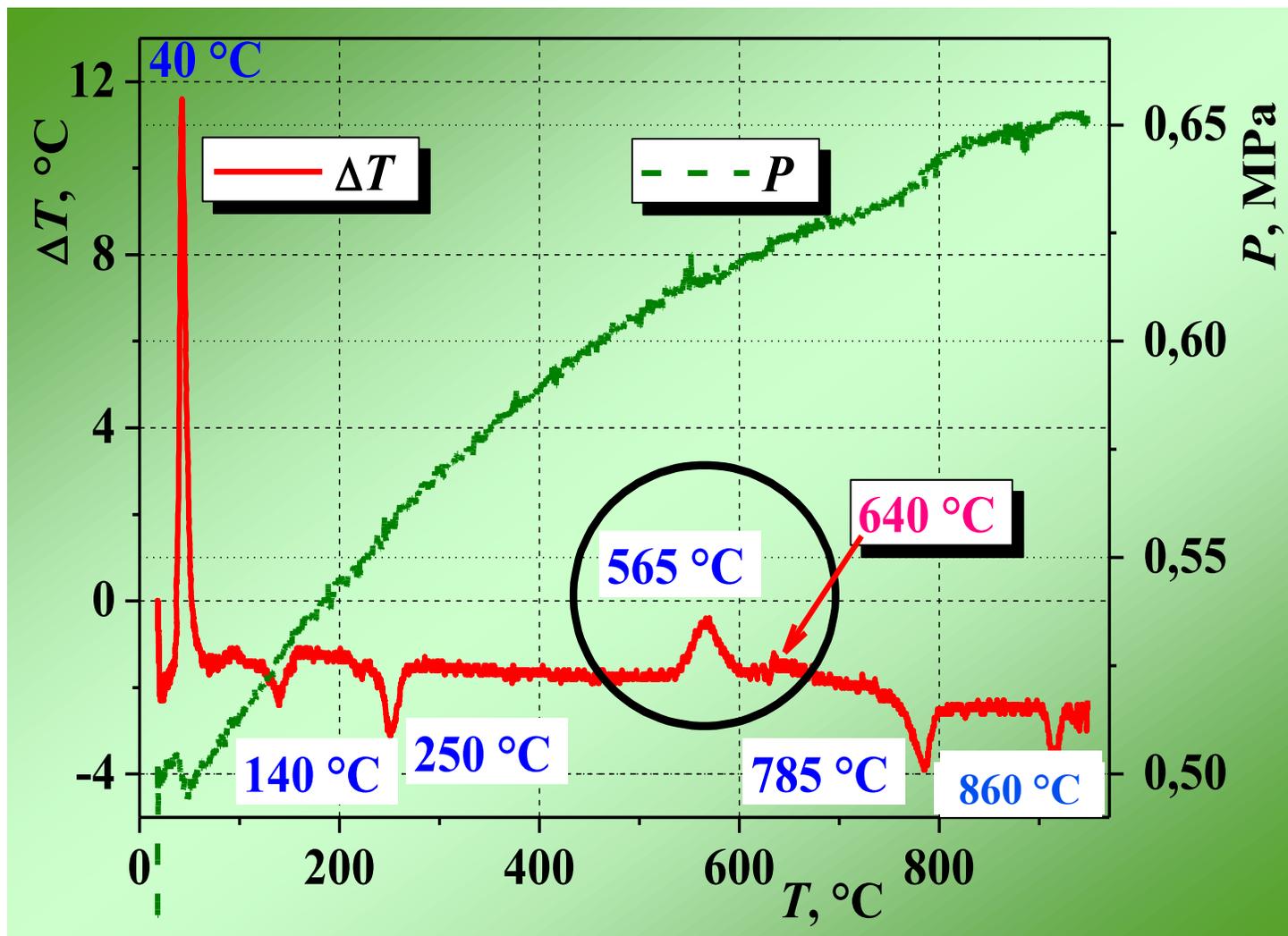
LITERATURE DATA



XRD patterns for SmCo_5 alloy:

- (i) starting alloy;
- (ii) (ii) after HD under 2 MPa;
- (iii) (iii) reactive milling in hydrogen.

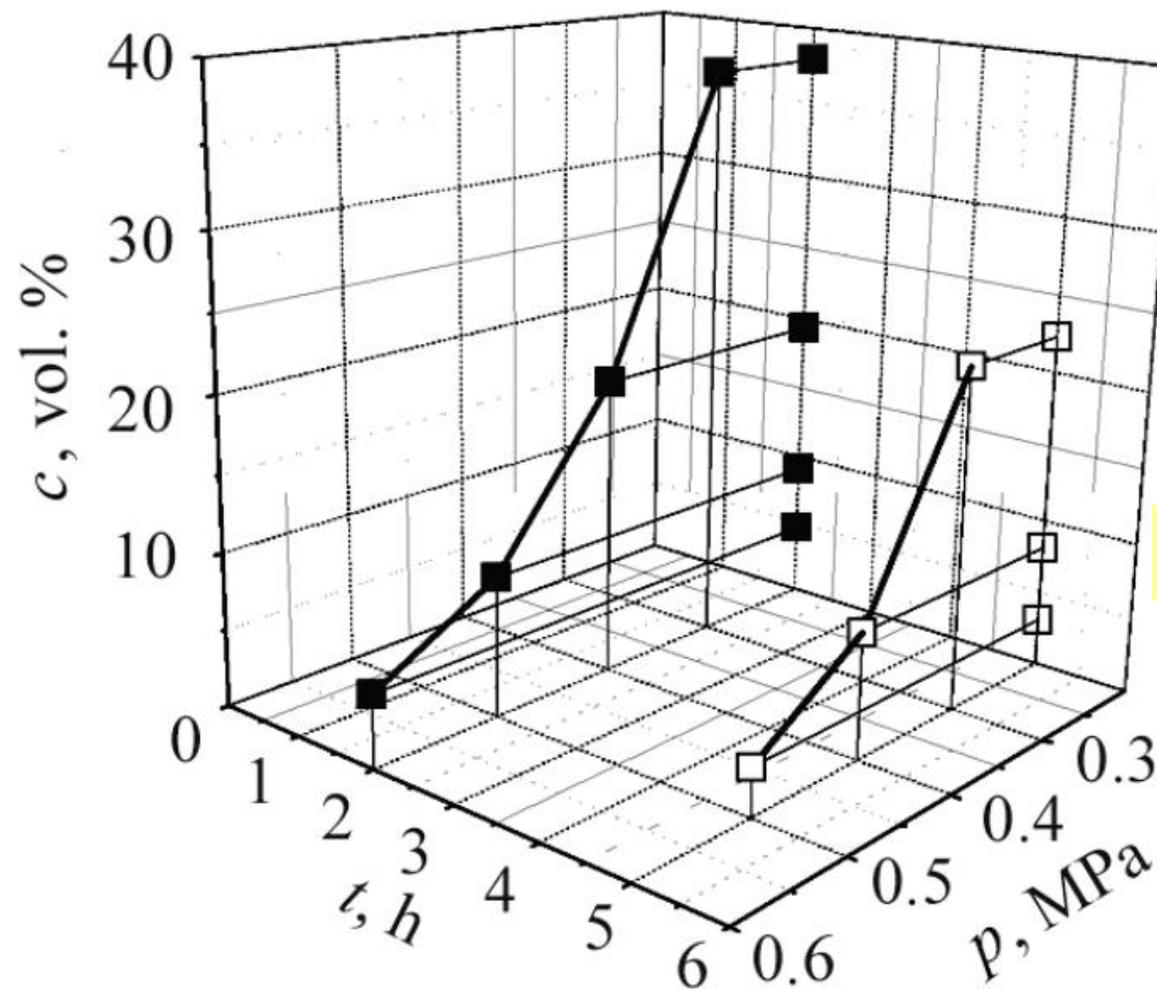
TERMS OF THE HDDR PROCESS IN SmCo_5 ALLOY



DTA curves for $\text{SmCo}_5\text{-H}_2$
under hydrogen pressures
of 0.5 MPa

TERMS OF THE HDDR PROCESS IN SmCo_5 ALLOY

- (c) amount of the SmCo_5 phase
- (p) hydrogen pressure
- (t) duration of reaction



Conventional
HD (640 °C)

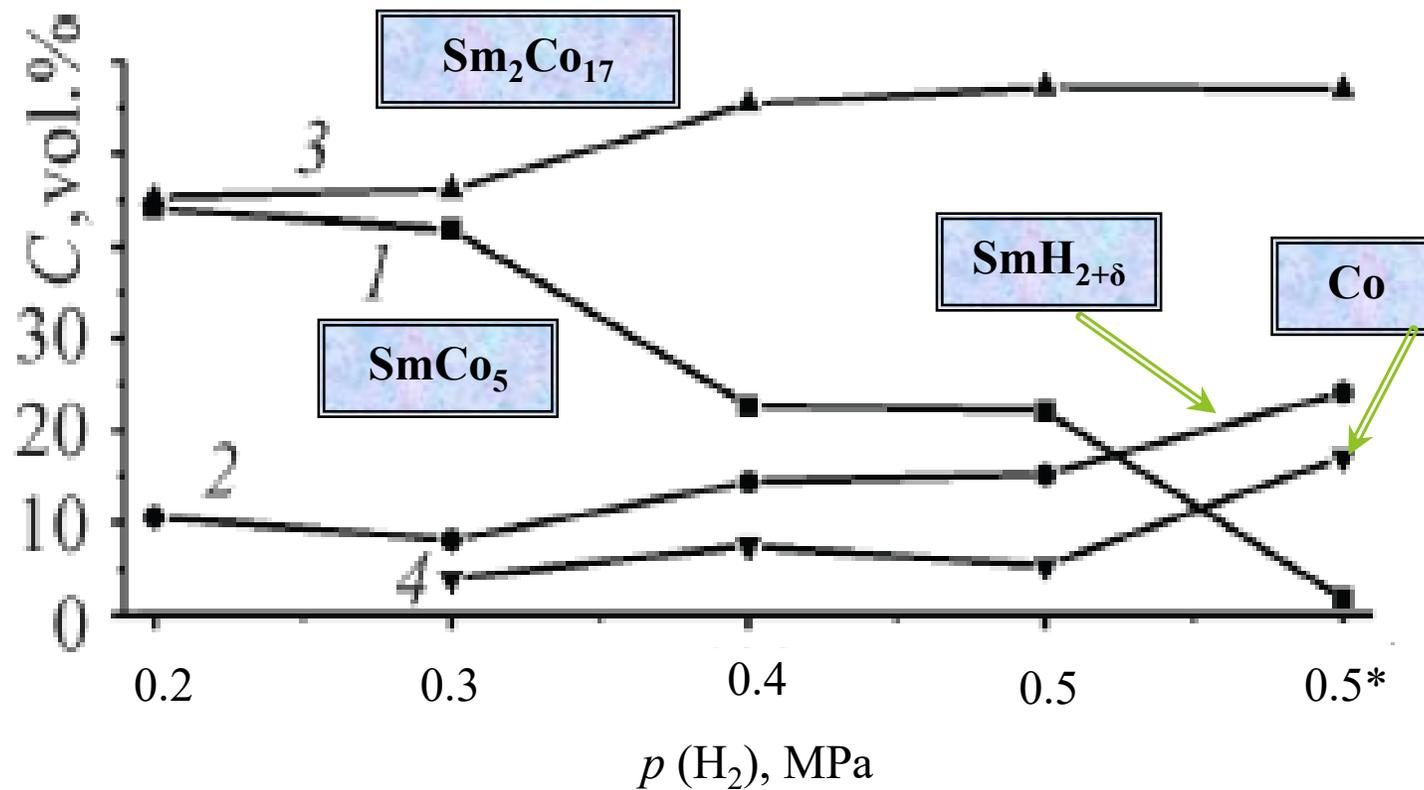


TERMS OF THE HDDR PROCESS IN SmCo_5 ALLOY

The phase composition of the SmCo_5 -based alloy after disproportionation in hydrogen

Solid HD, 700 °C,
holding time is 2 h

$\tau = 0$ h

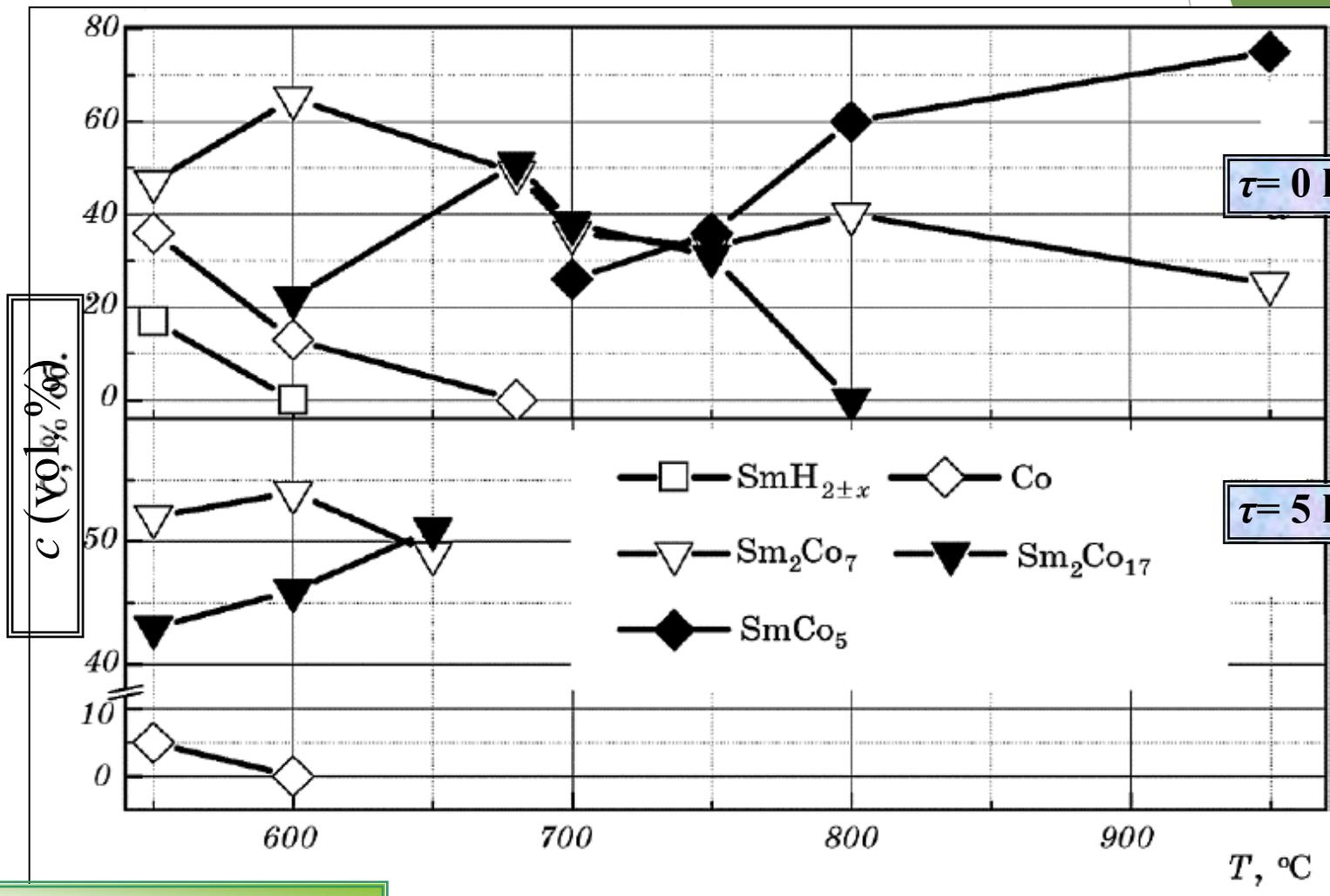


* - the holding time is 5 h

TERMS OF THE HDDR PROCESS IN SmCo_5 ALLOY

Phase composition
of SmCo_5 -based
alloy after
recombination

Conventional HDDR,
HD: 0.5 MPa, 640 °C, 5 h

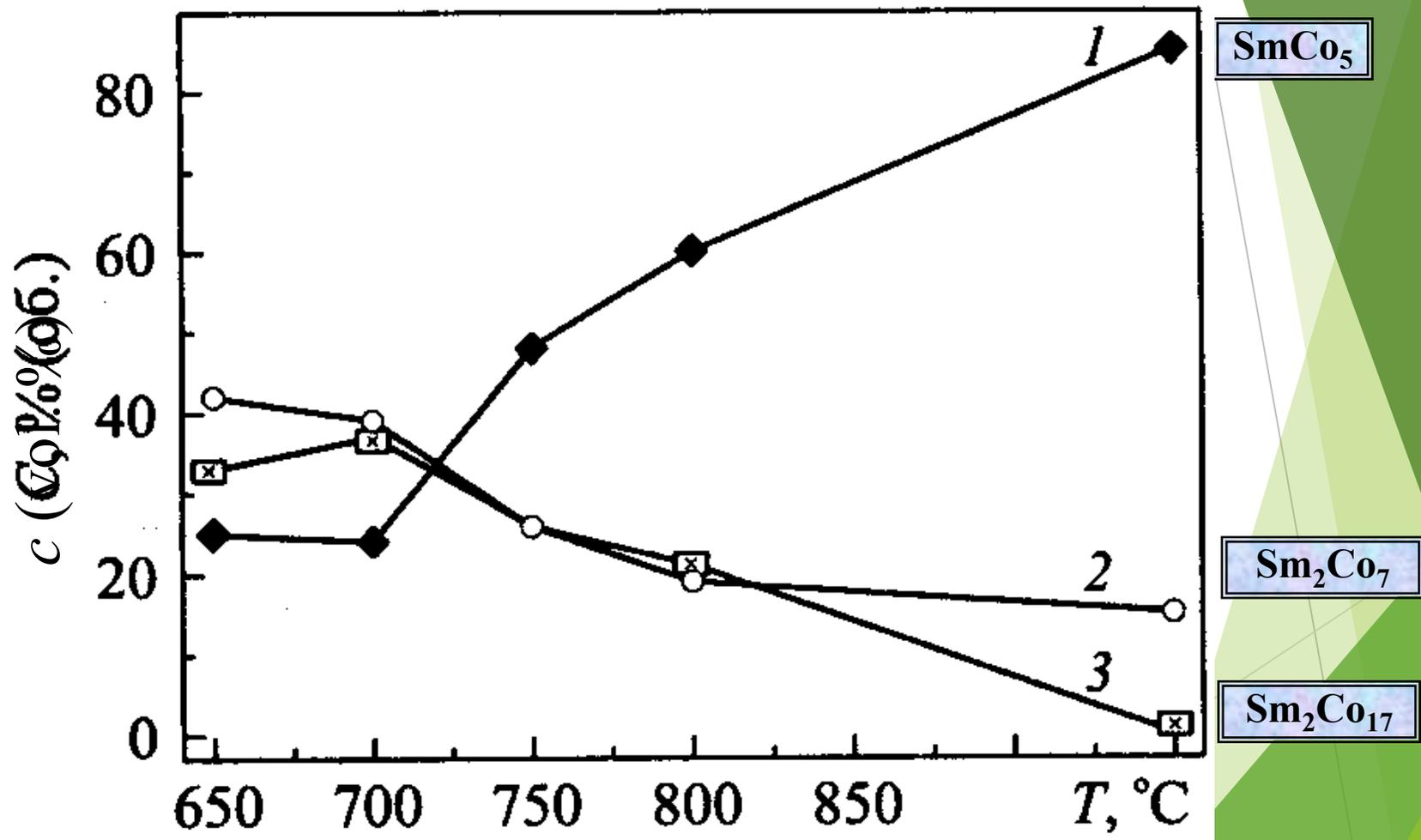


I.I. Bulyk and A.M. Trostianchyn, Metallofiz. Noveishie Tekhnol., 38 (2016) 511—519 (in Ukrainian), <https://doi.org/10.15407/mfint.38.04.0511>.

TERMS OF THE HDDR PROCESS IN SmCo_5 ALLOY

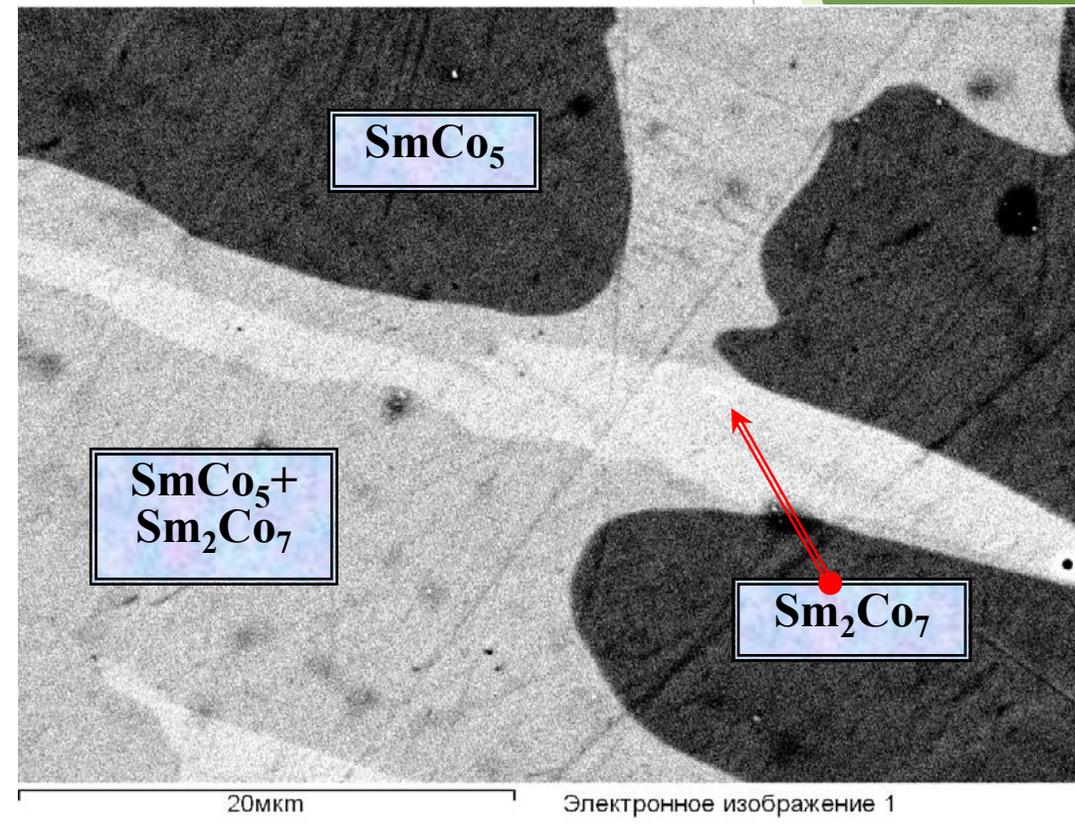
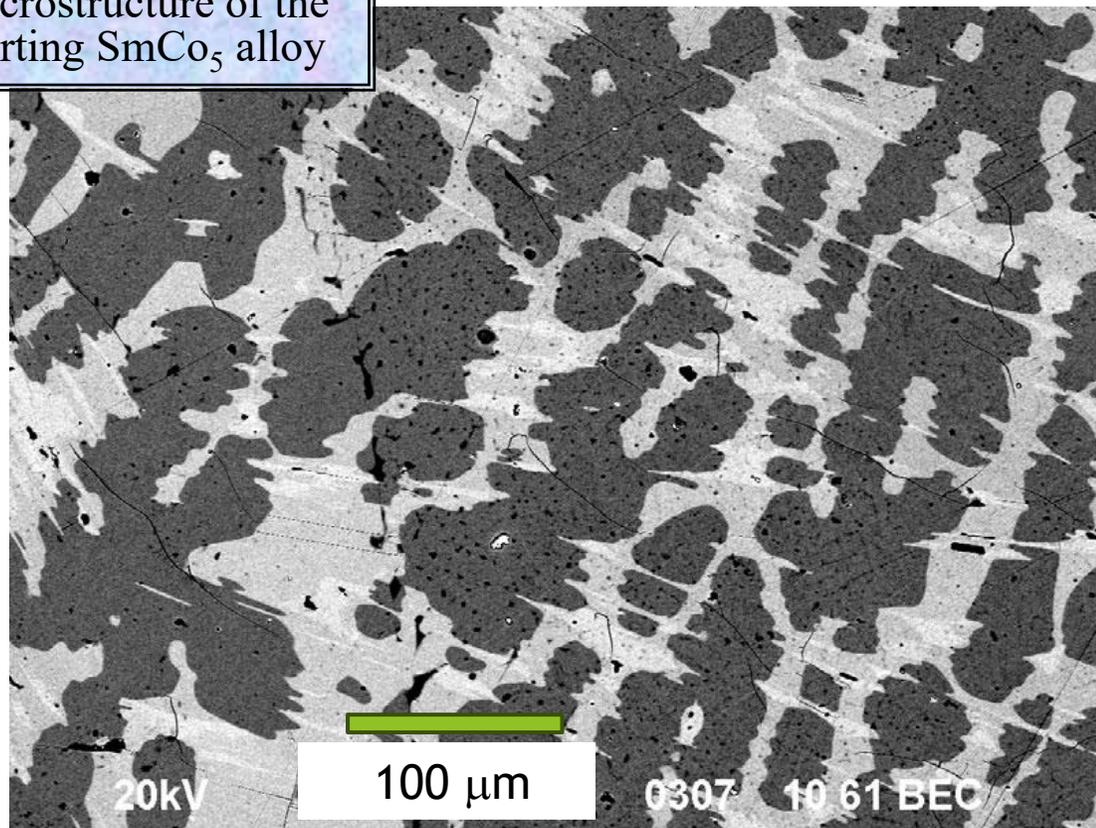
Phase composition of SmCo_5 -based alloy after recombination

Solid HDDR, HD:
0.4 MPa, 650°C, 2 h



FEATURES OF THE MICROSTRUCTURE OF THE SmCo_5 ALLOY DURING HDDR

Microstructure of the starting SmCo_5 alloy

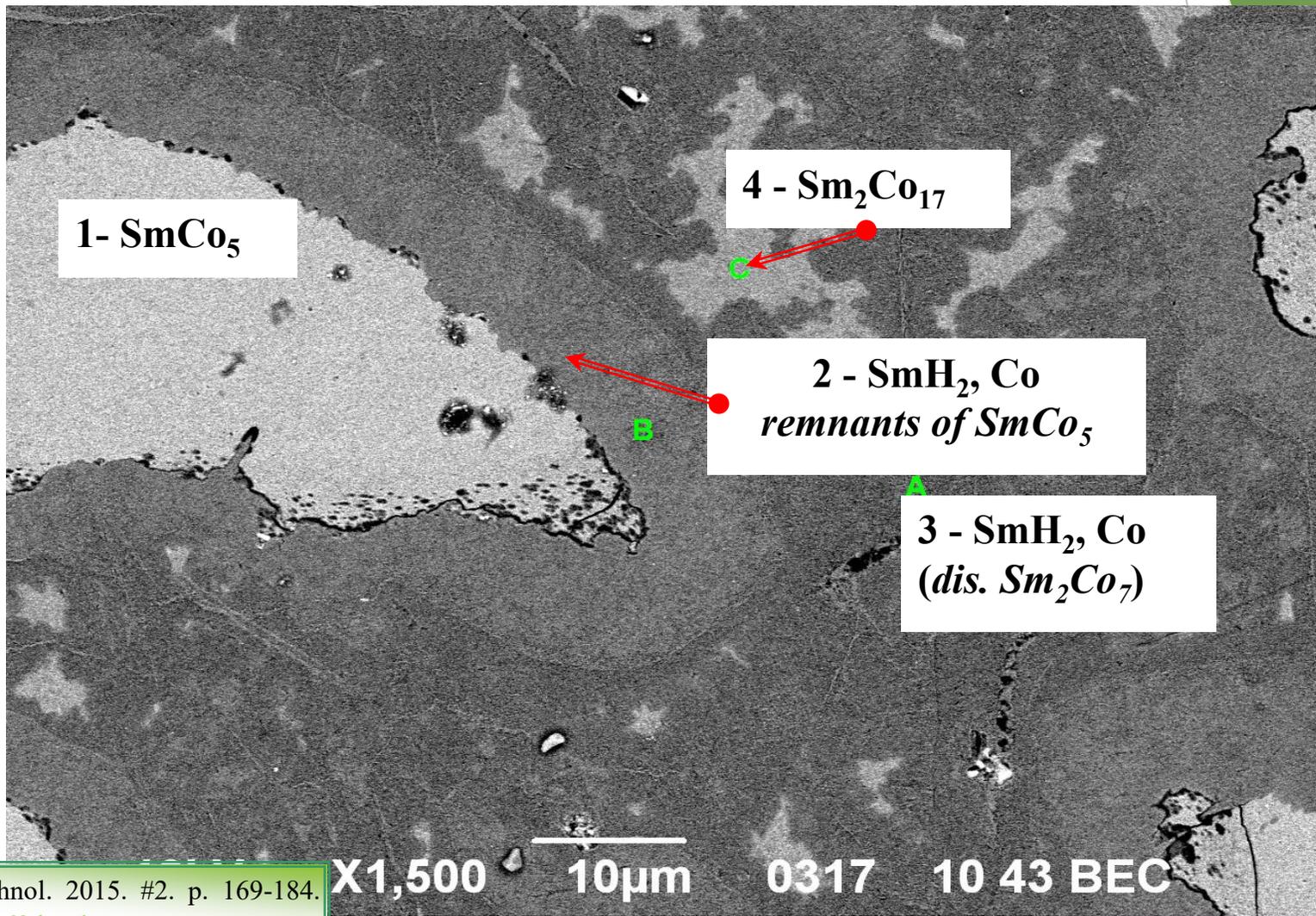


I.I. Bulyk, et al, Metallofiz. Noveishie Tekhnol. 2015. #2. p. 169-184. <http://mfint.imp.kiev.ua/ua/abstract/v37/i02/0169.html>.

FEATURES OF THE MICROSTRUCTURE OF THE SmCo_5 ALLOY DURING HDDR

SmCo_5 ALLOY
AFTER solid HD
partially
disproportionated

solid-HD:
0.5 MPa,
640 °C, 5 h.

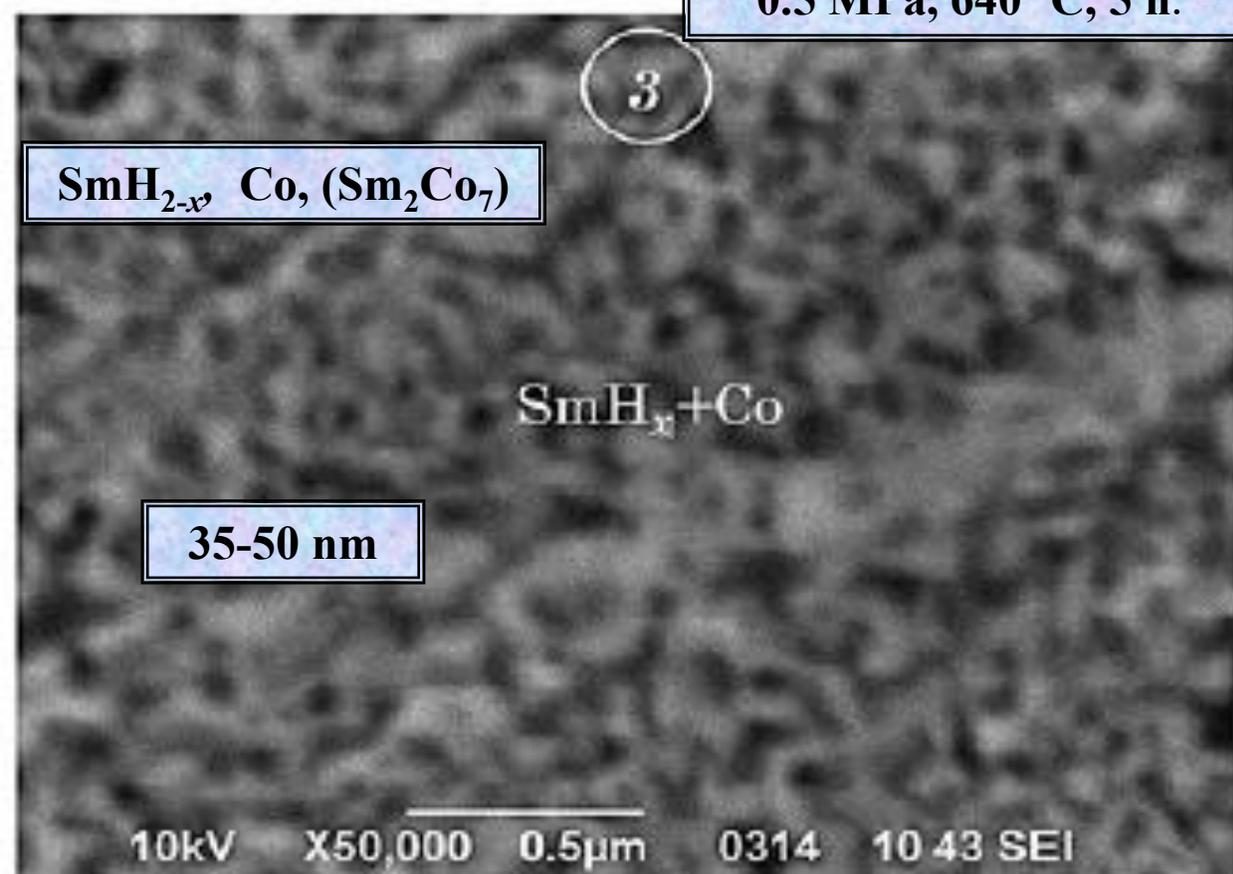
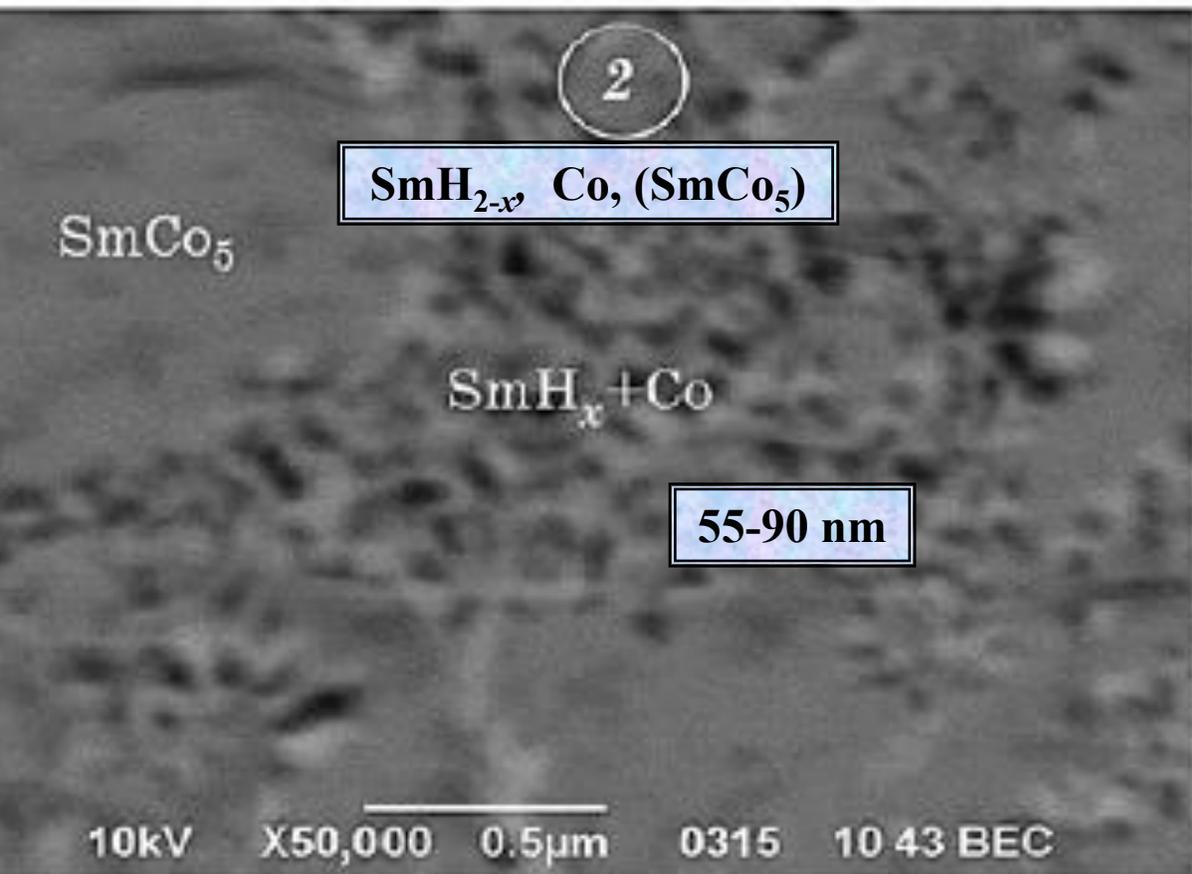


I.I. Bulyk, et all Metallofiz. Noveishie Tekhnol. 2015. #2. p. 169-184.
<http://mfint.imp.kiev.ua/ua/abstract/v37/i02/0169.html>.

FEATURES OF THE MICROSTRUCTURE OF THE SmCo_5 ALLOY DURING HDDR

SmCo_5 ALLOY AFTER solid HD partially disproportionated

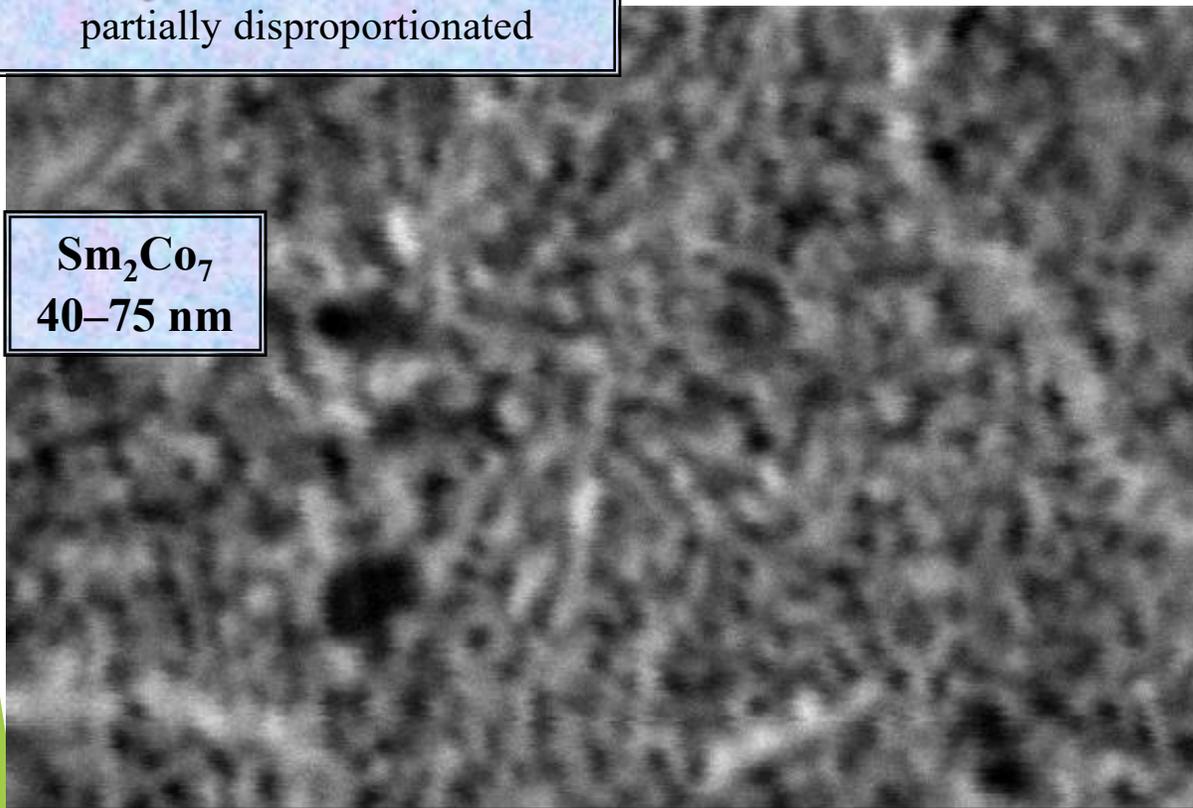
**solid-HD:
0.5 MPa, 640 °C, 5 h.**



I.I. Bulyk, et al, Metallofiz. Noveishie Tekhnol. 2015. #2. p. 169-184. <http://mfint.imp.kiev.ua/ua/abstract/v37/i02/0169.html>.

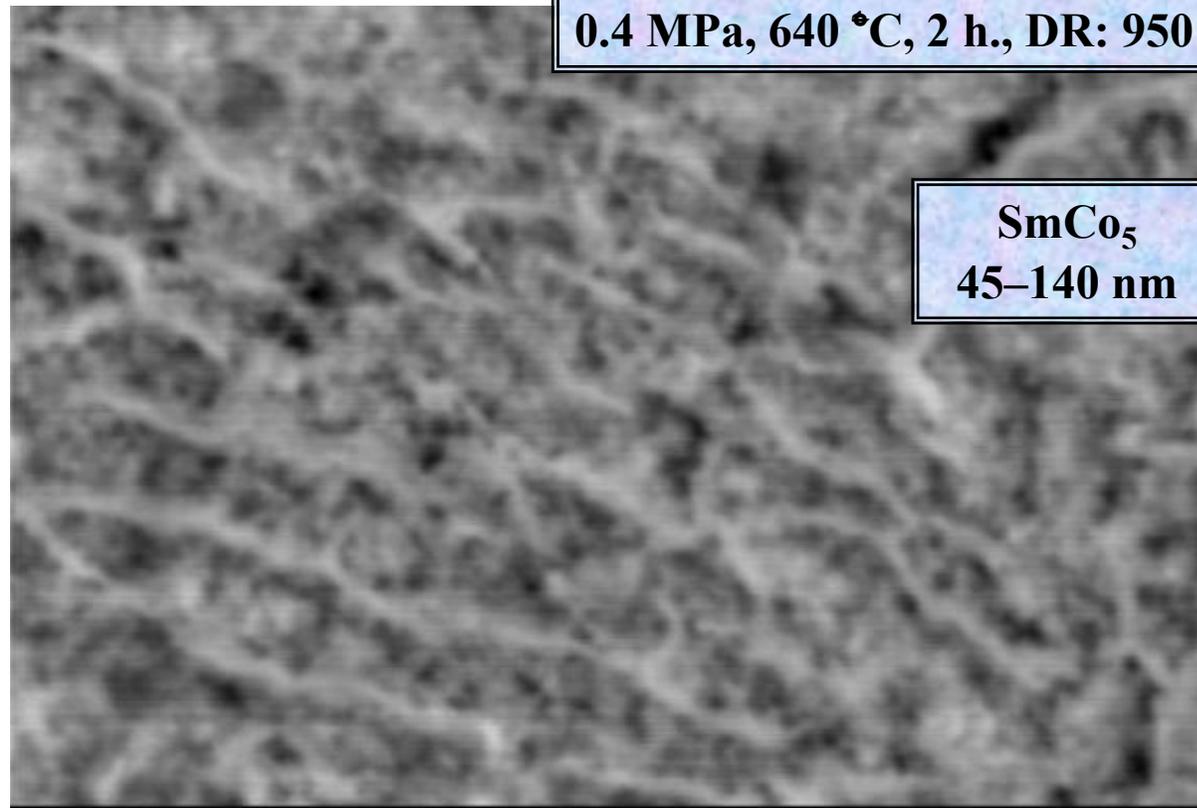
FEATURES OF THE MICROSTRUCTURE OF THE SmCo_5 ALLOY DURING HDDR

SmCo_5 AFTER solid HDDR
partially disproportionated



Sm_2Co_7
40–75 nm

solid-HD.
0.4 MPa, 640 °C, 2 h., DR: 950 °C

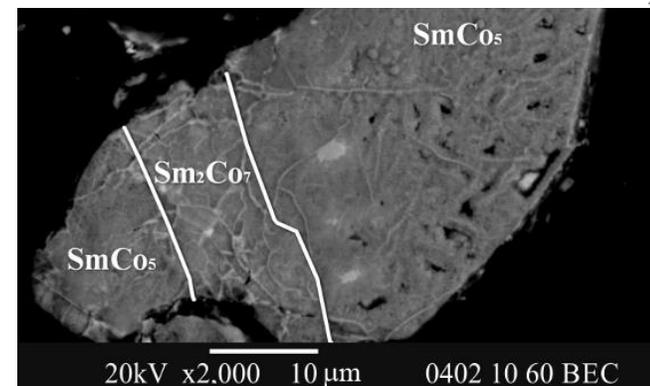
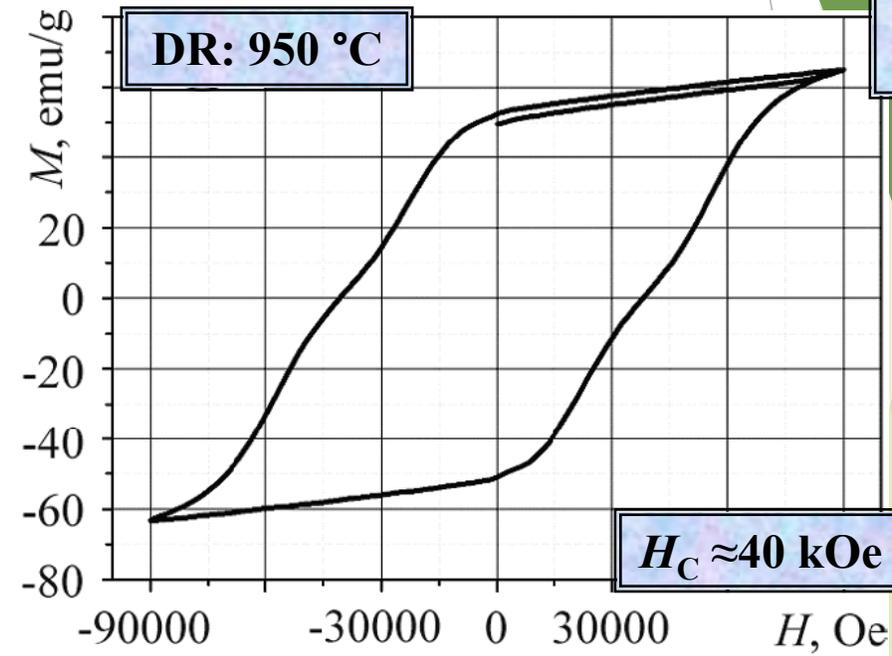
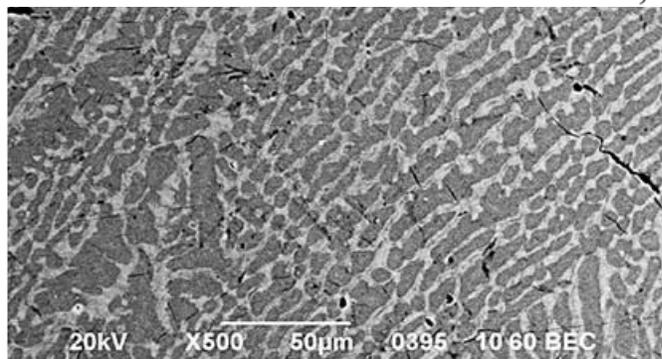
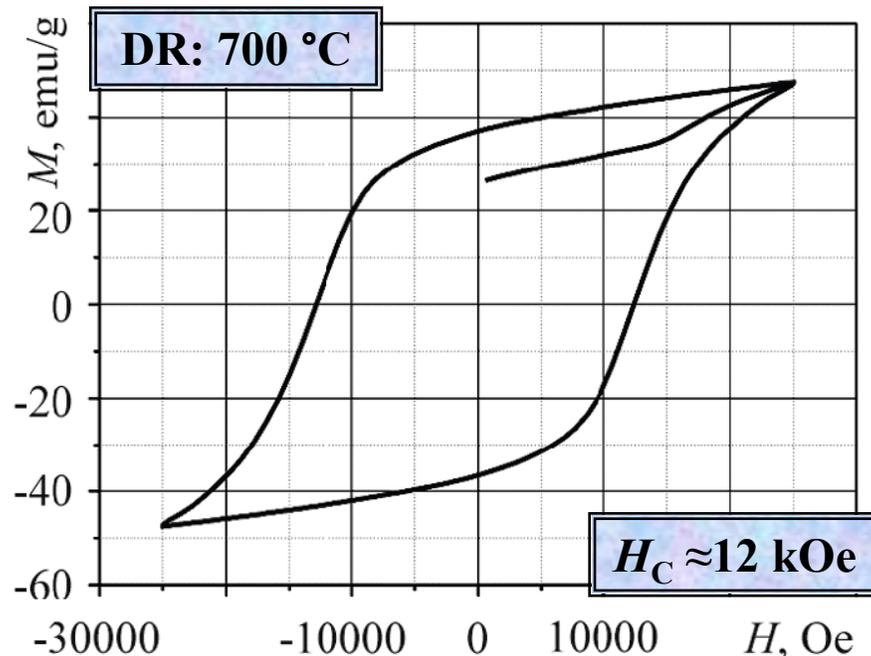


SmCo_5
45–140 nm

10kV x40,000 0.5 μm 0402 10 40 SEI

20kV x8,000 0.2 μm 0402 10 60 BEC

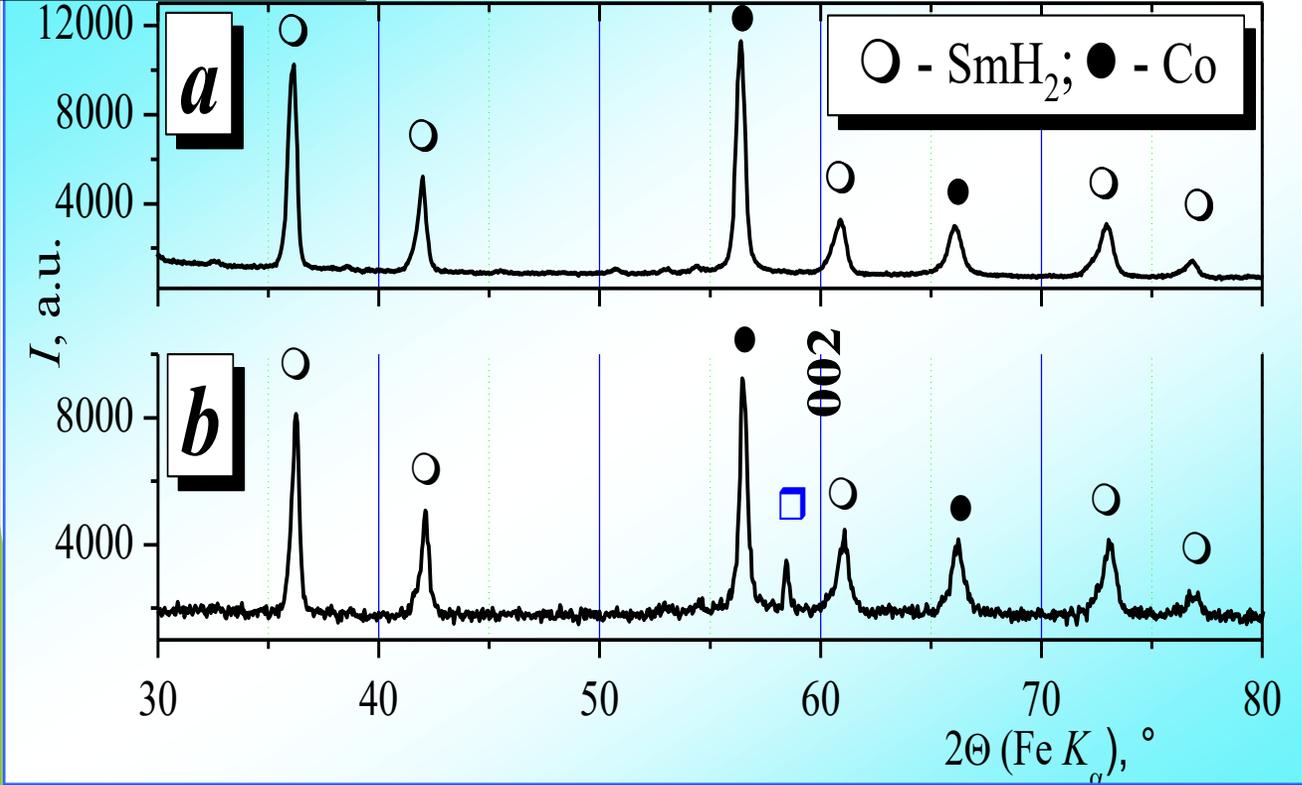
Magnetic properties of the SmCo_5 alloy powder after solid HDDR



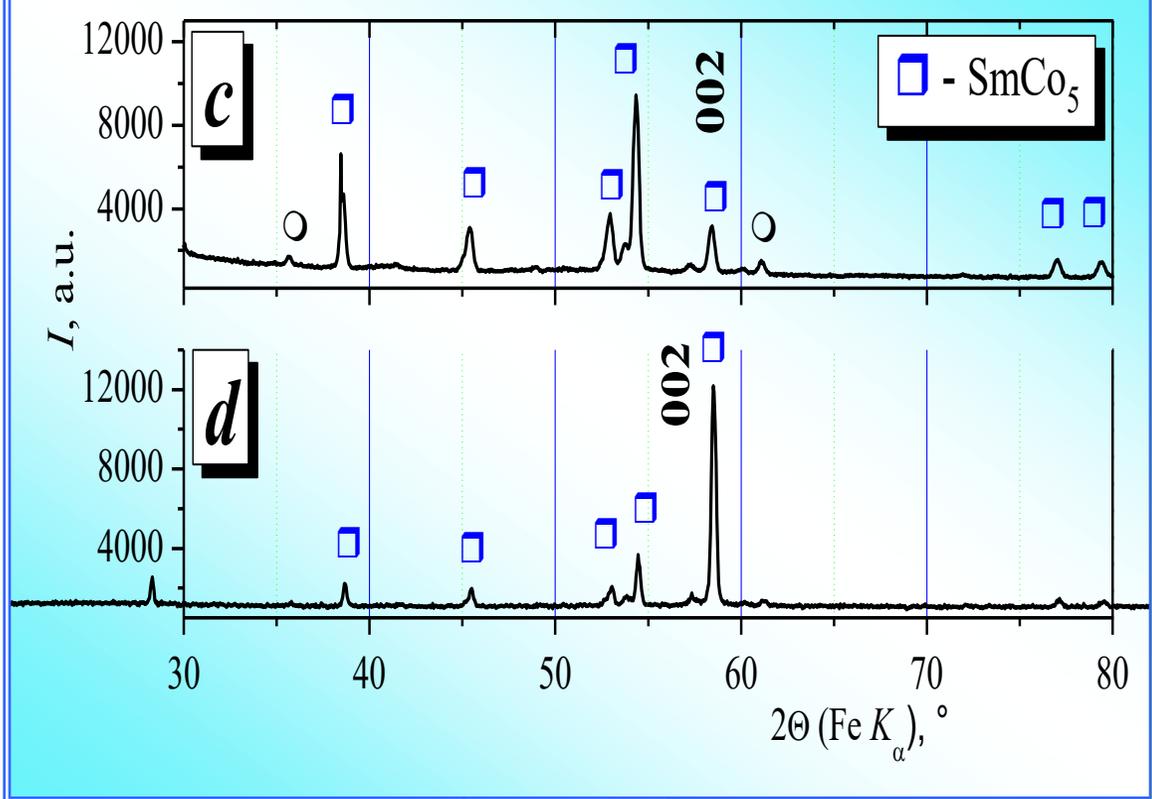
solid-HD:
0.4 MPa,
640 °C, 2 h.

TEXTURE MEMORY MECHANISM IN Sm-Co MATERIALS AFTER HDDR

SmCo₅ after HD:
a and *b*



SmCo₅ after HDDR:
c and *d*

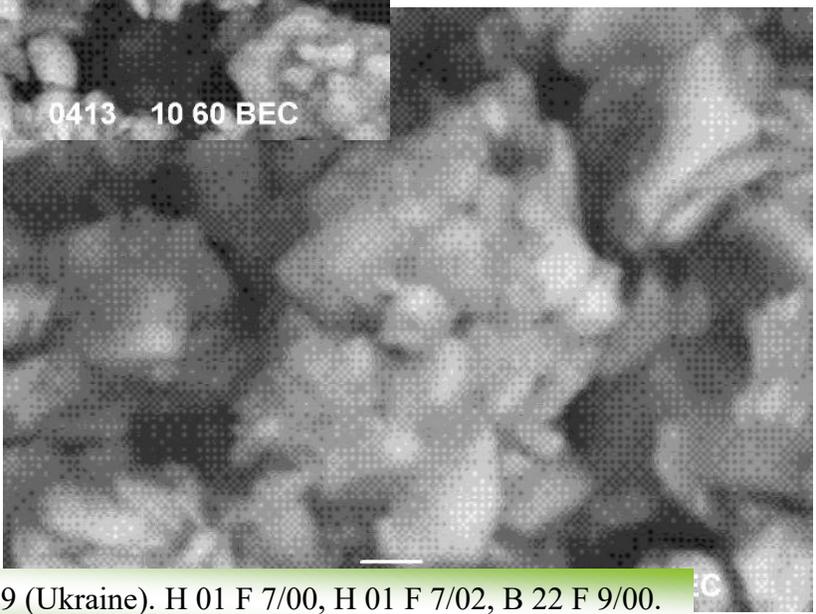
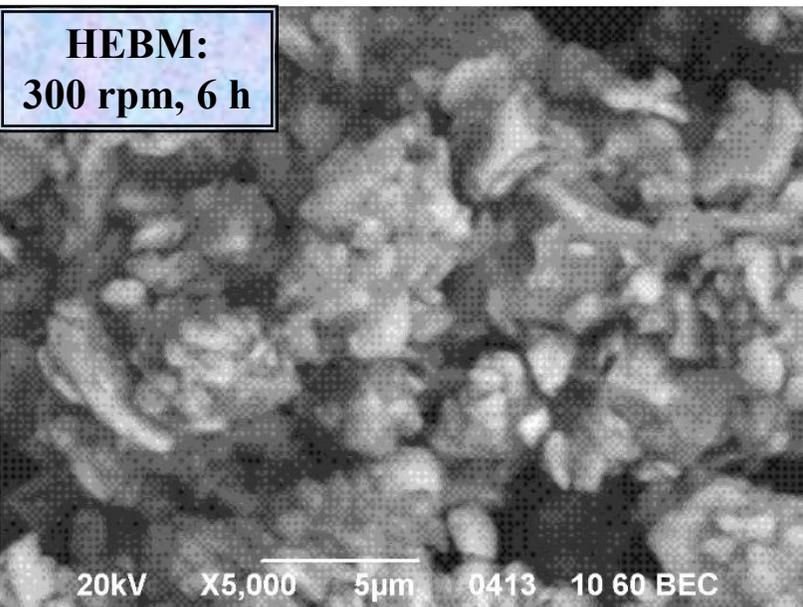


XRD patterns measured for:
a and *c* – random powders; *b* and *d* – powders oriented in magnetic field.

Preliminary Results of Sintering SmCo_5 Magnetic Materials Using the HDDR Process

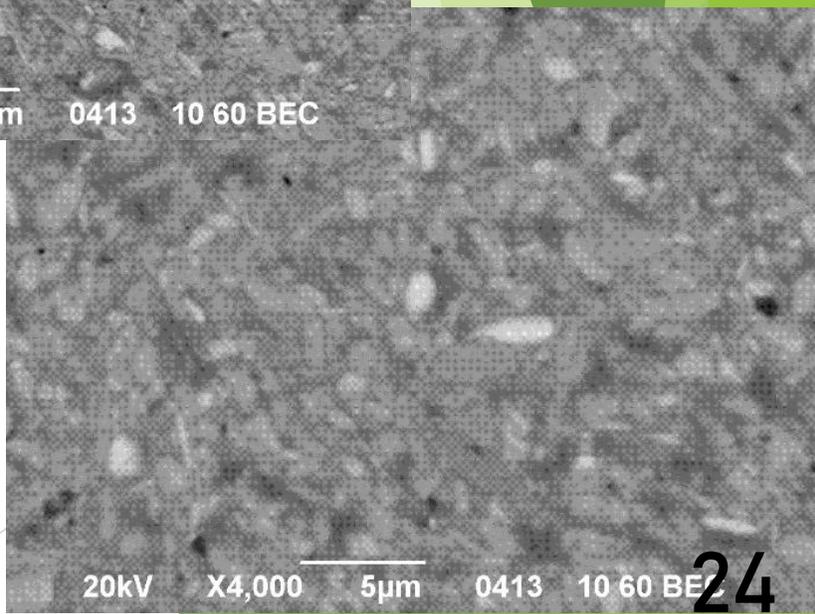
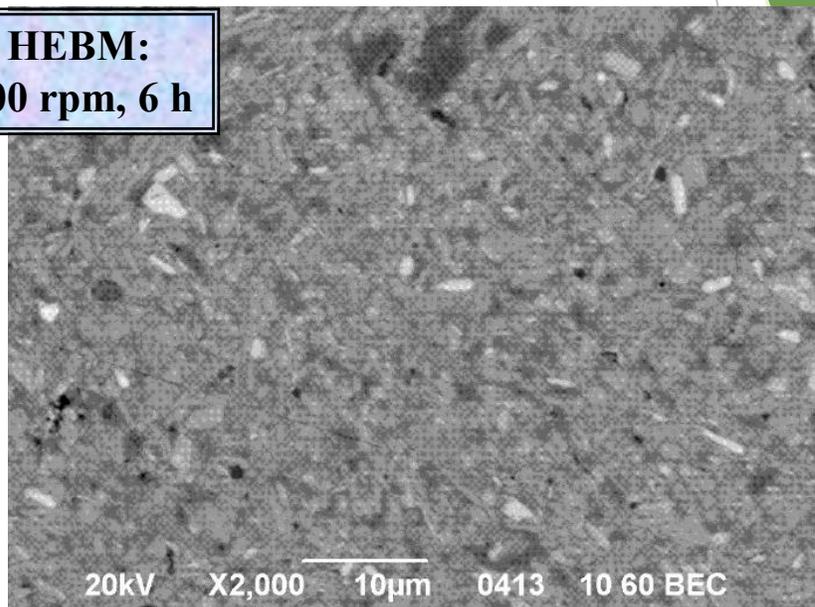
Morphology of $\text{Sm}(\text{Co},\text{Zr})_5$ powders after HEBM

HEBM:
300 rpm, 6 h

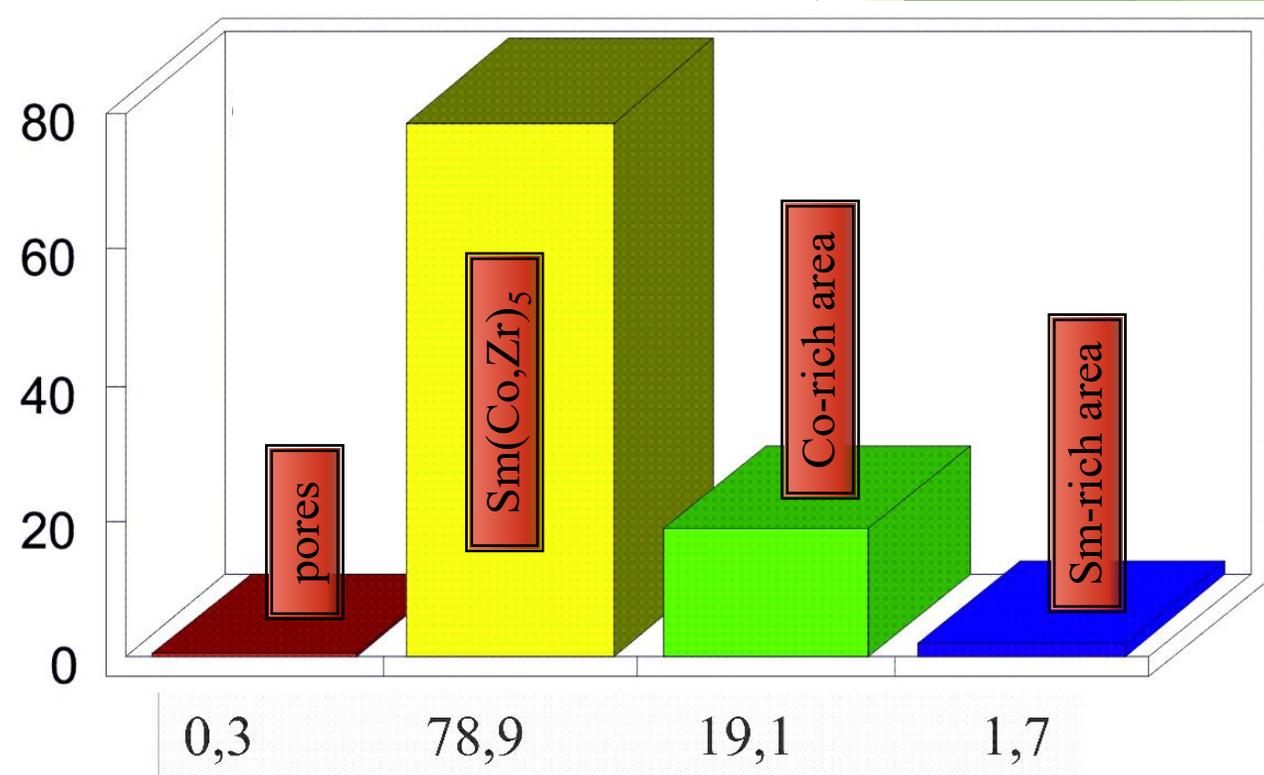
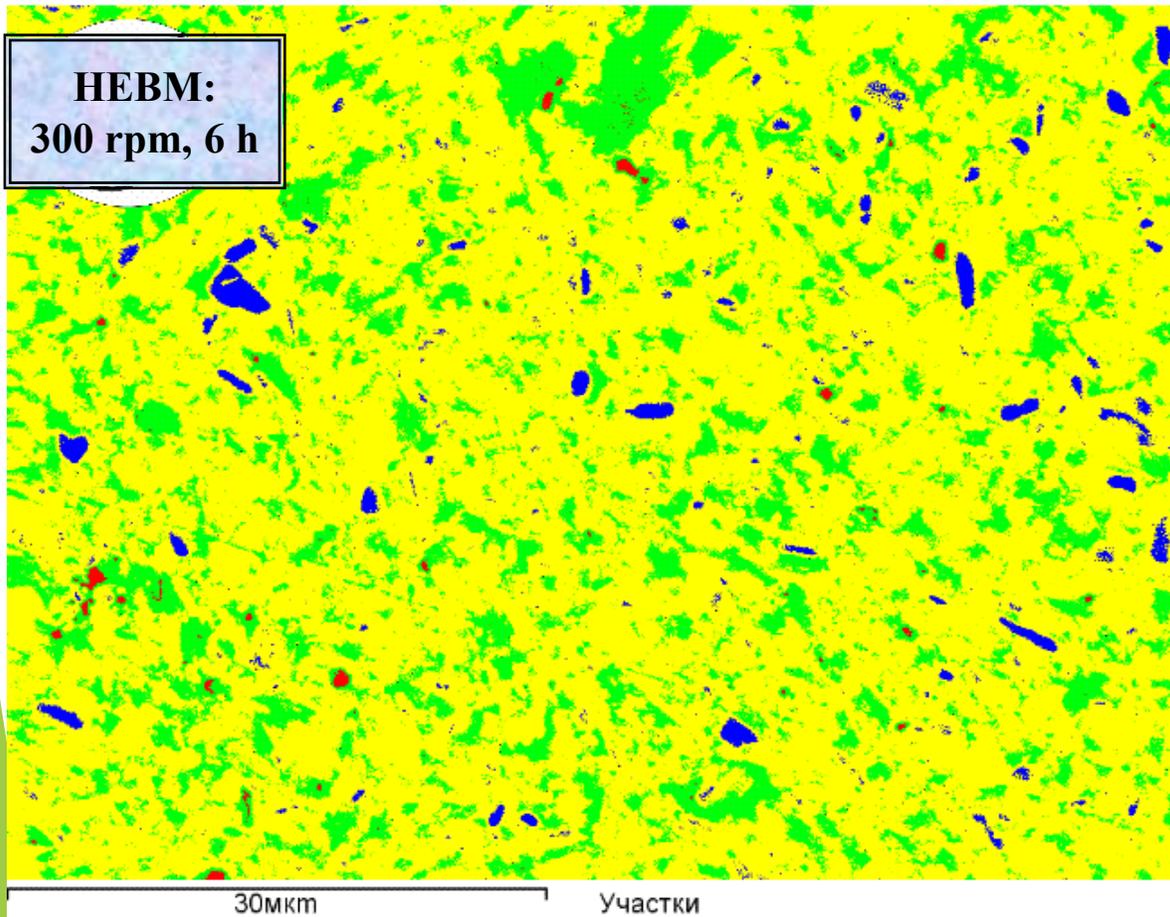


Microstructure of $\text{Sm}(\text{Co},\text{Zr})_5$ materials sintered by HDDR

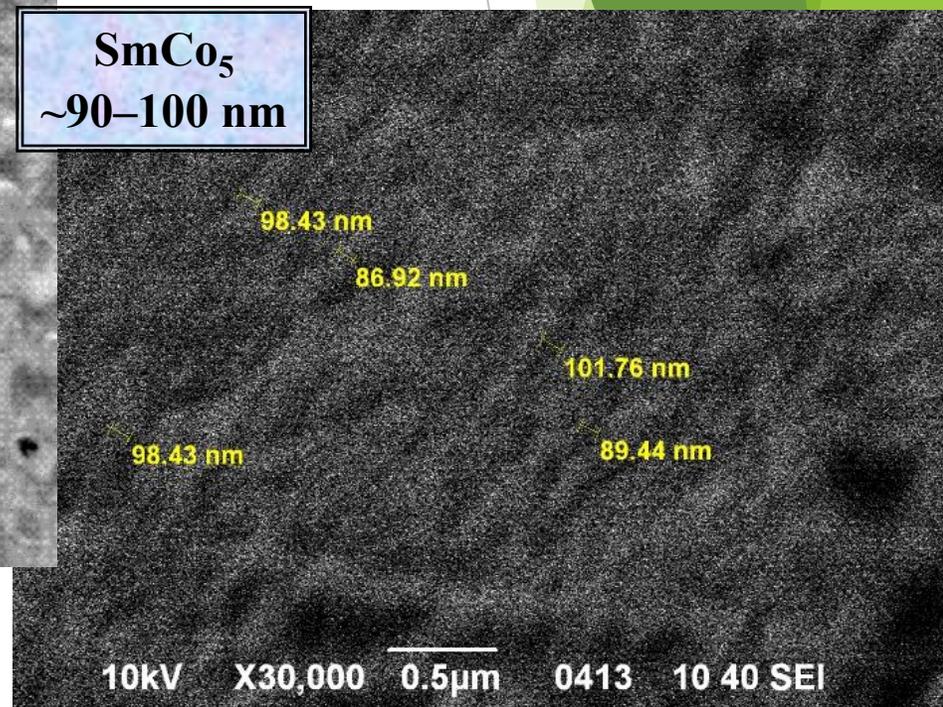
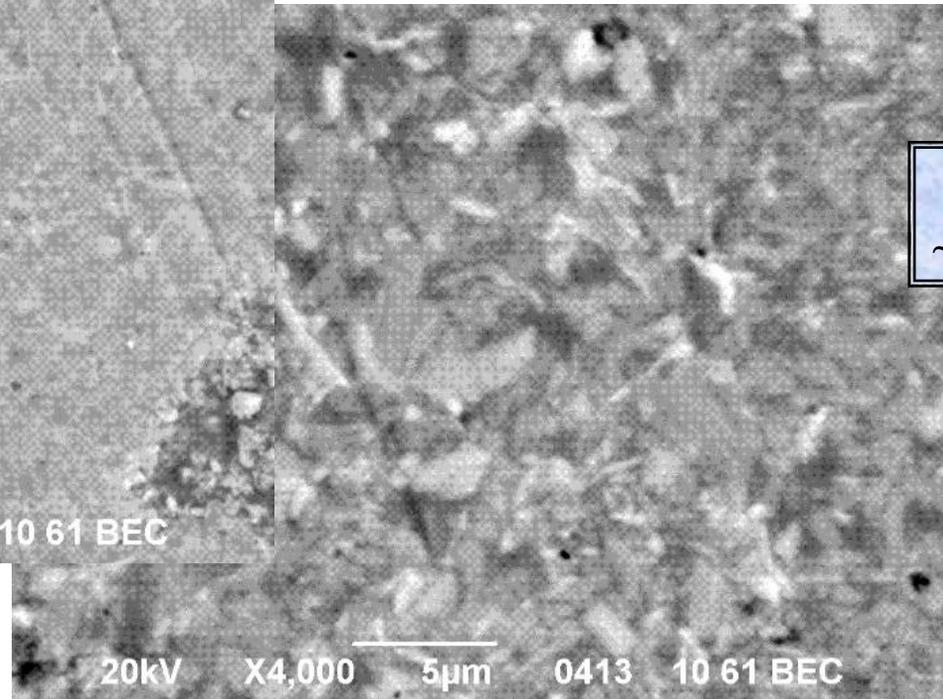
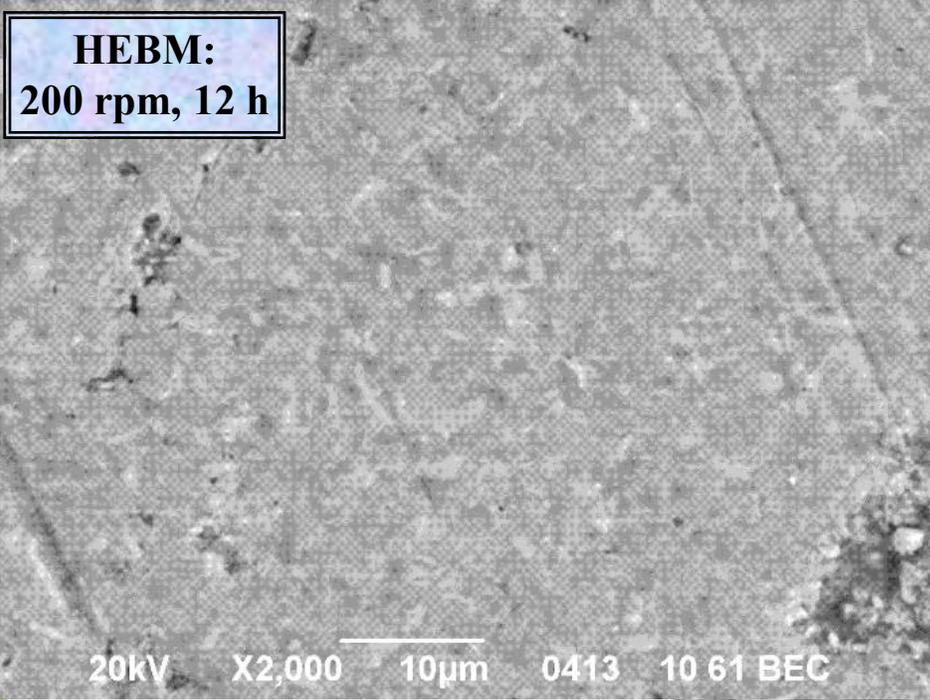
HEBM:
300 rpm, 6 h



Morphology and Ratio of microstructure components of $\text{Sm}(\text{Co,Zr})_5$ alloy sintered by HDDR

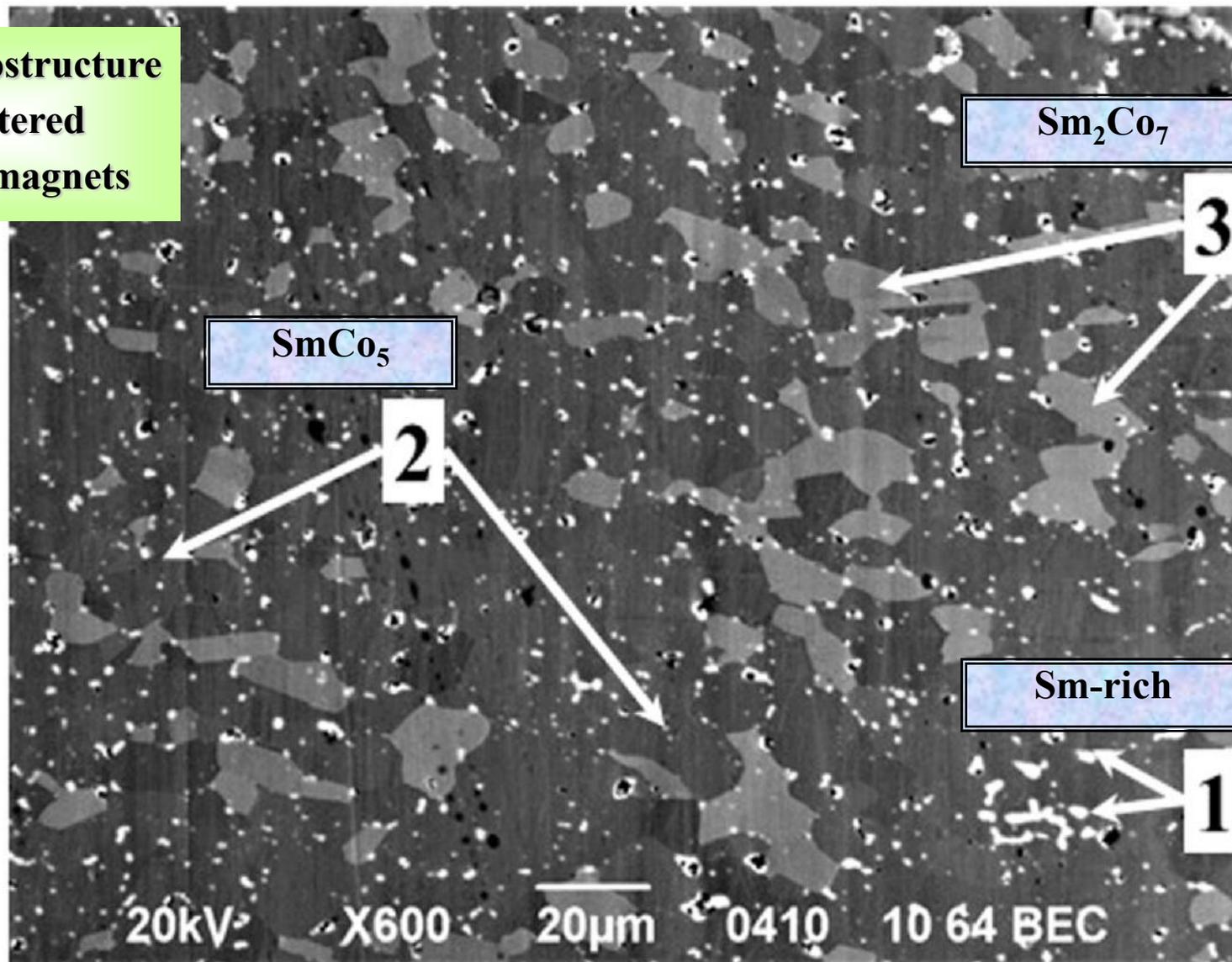


Microstructure of $\text{Sm}(\text{Co},\text{V})_5$ alloy sintered by HDDR



POST-SINTERING TREATMENT OF SmCo_5 ALLOY BY HDDR

The microstructure of sintered SmCo_5 magnets



POST-SINTERING TREATMENT:

solid HD,
temperature of $650\text{ }^\circ\text{C}$,
without holding at this
temperature,
hydrogen pressure –
up to 1.1 Mpa ;

DR: vacuum

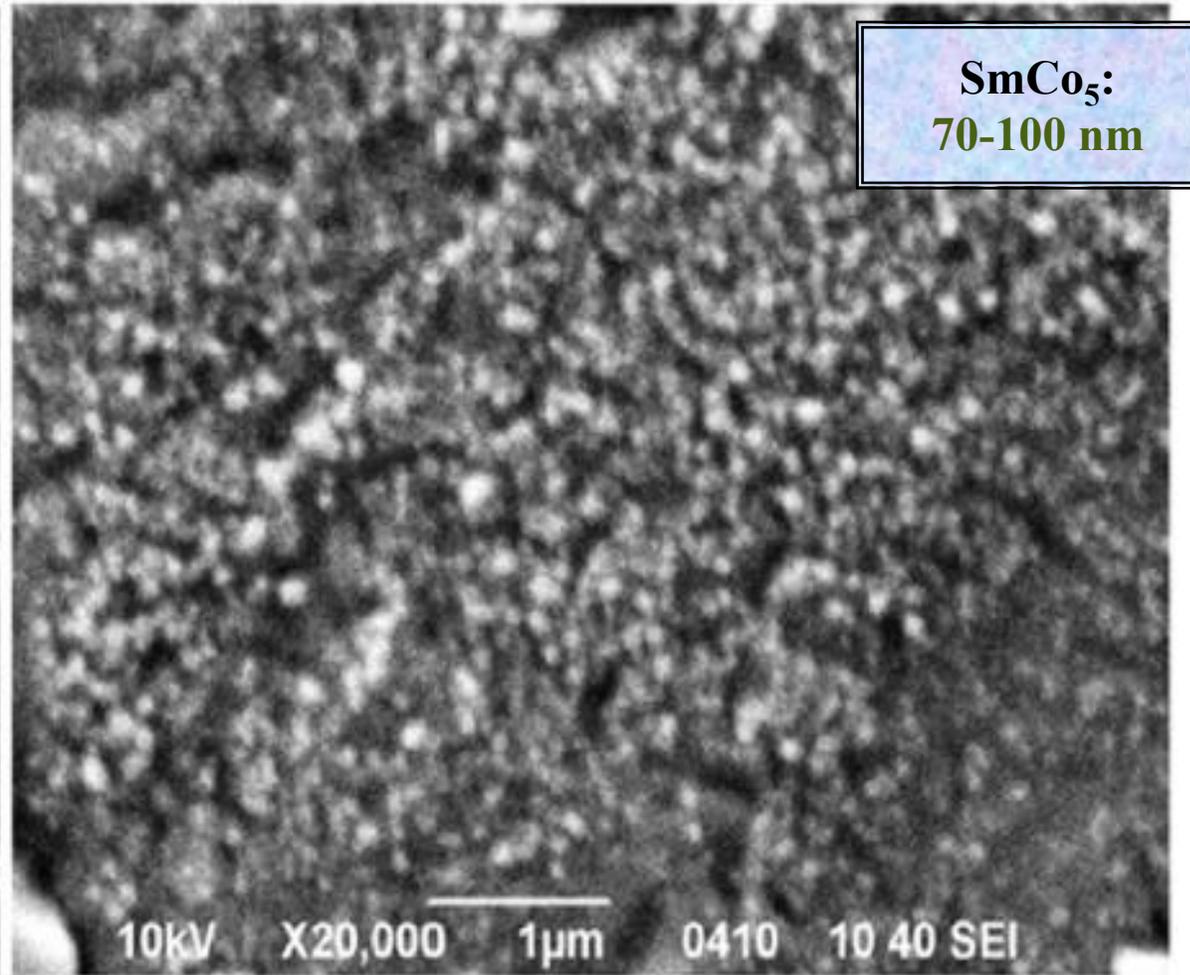
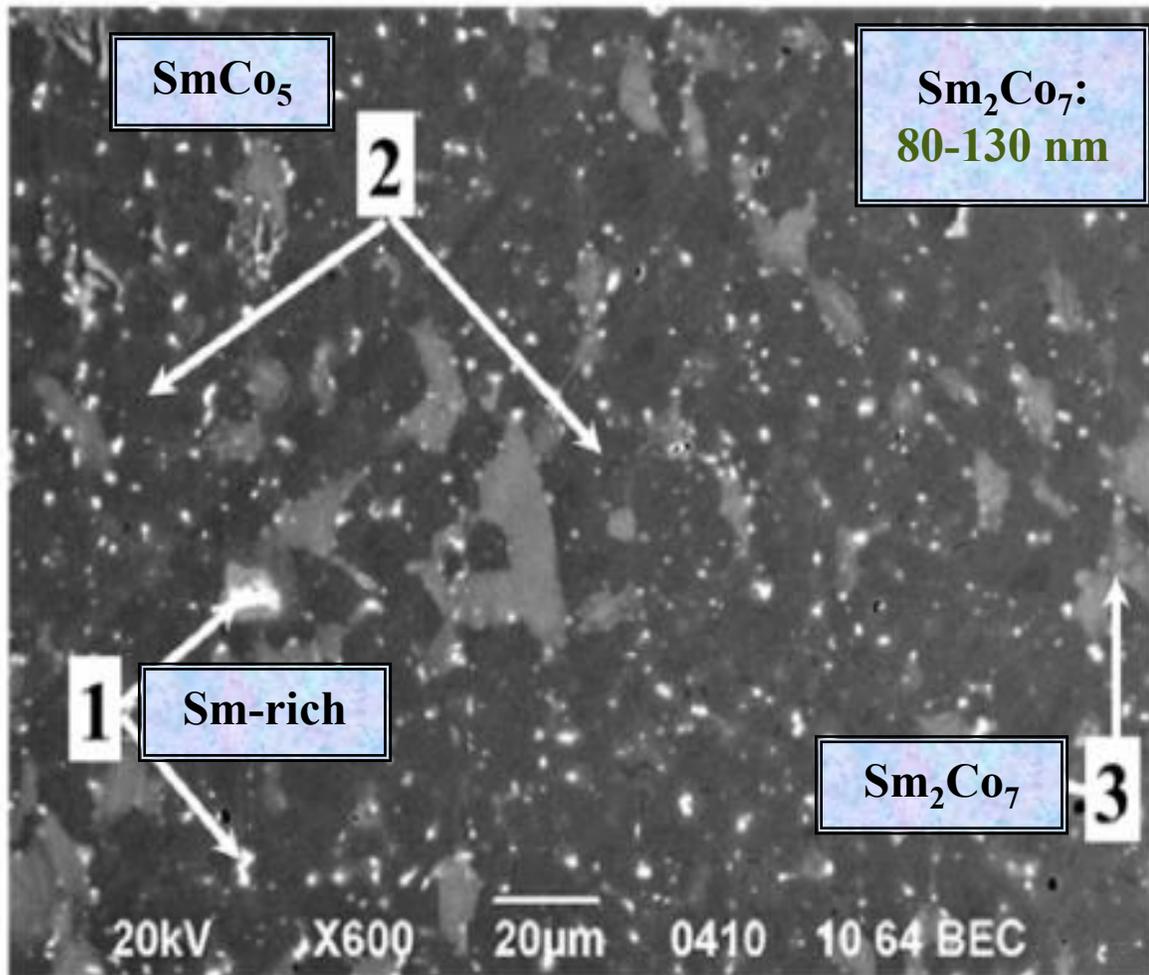
1 – $850\text{ }^\circ\text{C}$;

2 – $850\text{ }^\circ\text{C}$, 1 h;

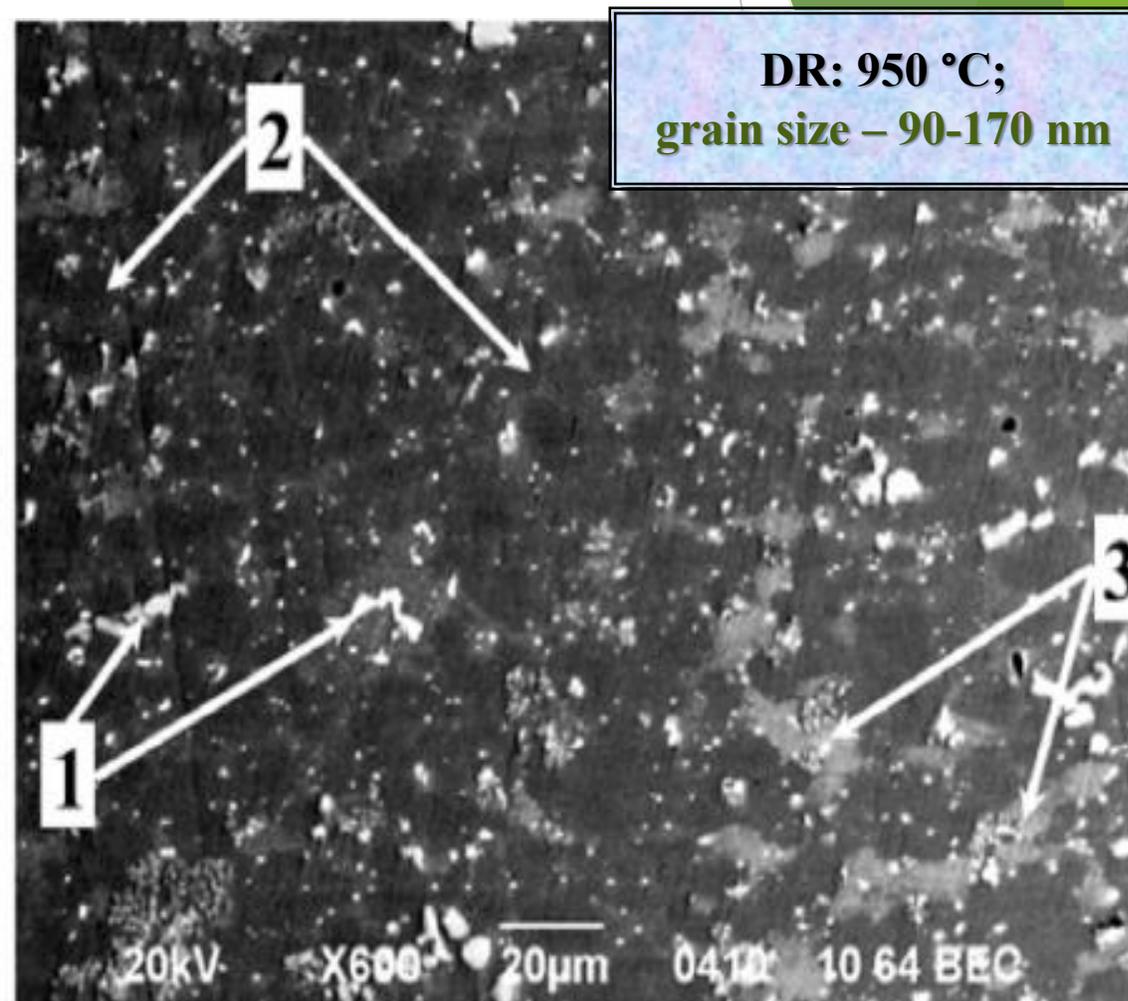
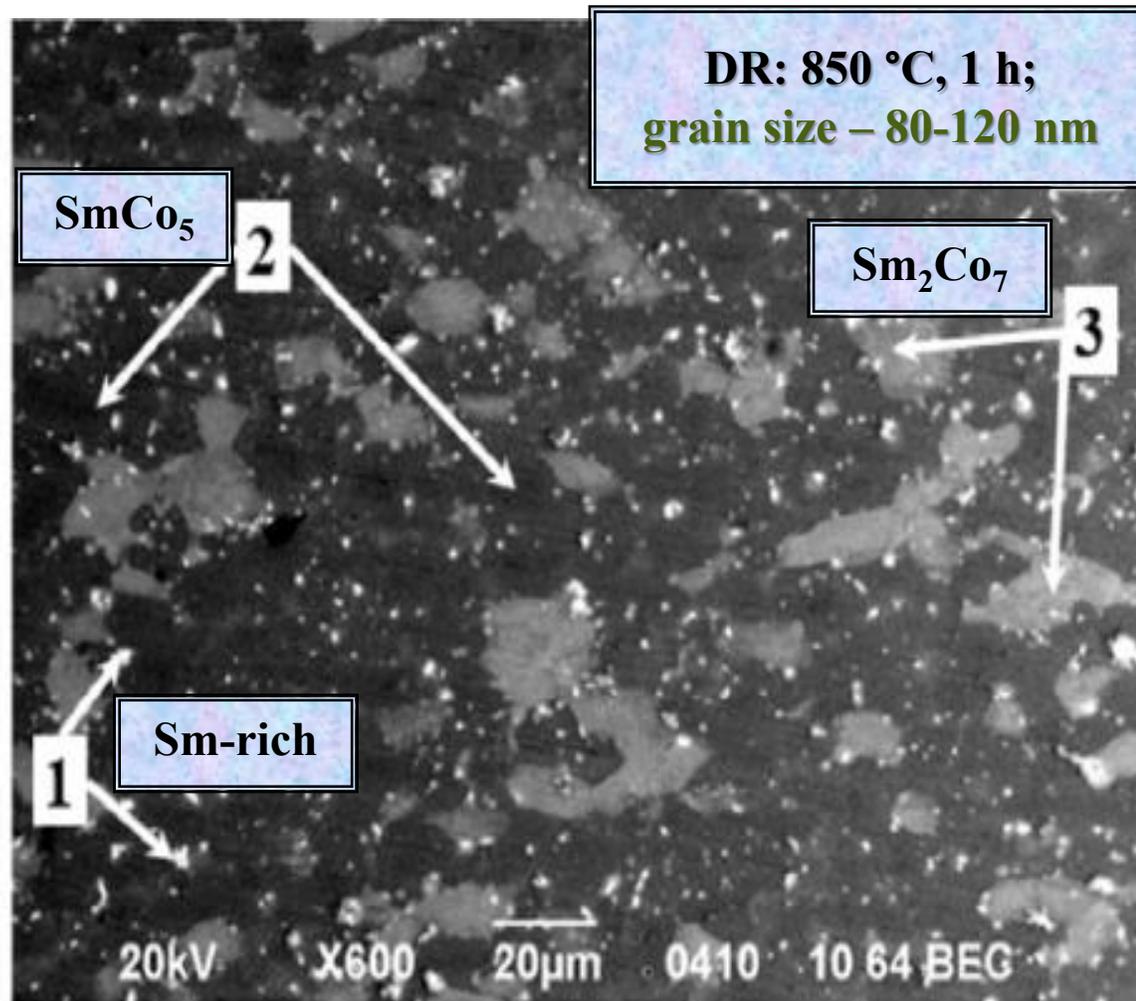
3 – $950\text{ }^\circ\text{C}$

Microstructure sintered SmCo_5 magnets after HDDR

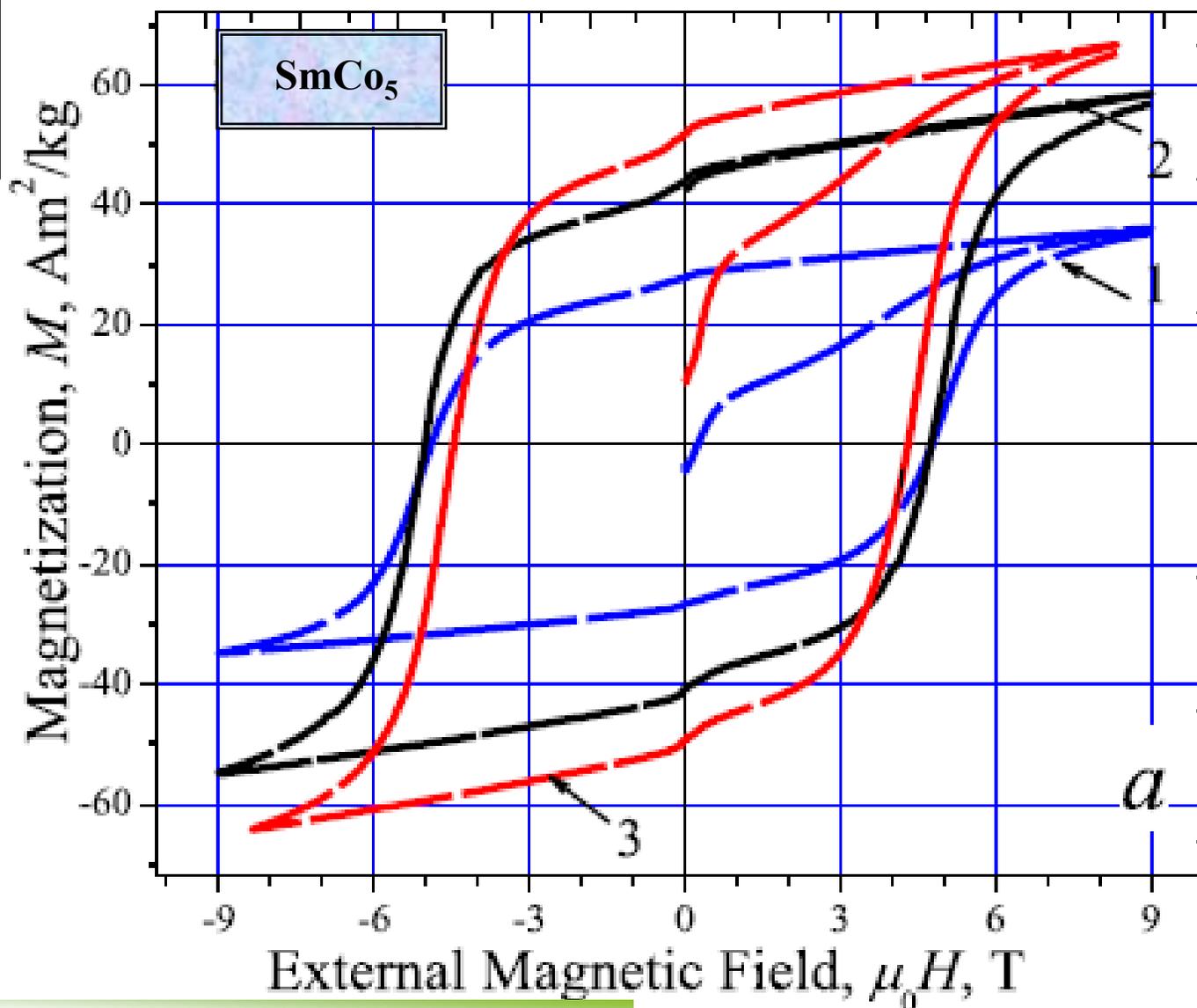
DR: 850 °C



Microstructure sintered SmCo_5 magnets after HDDR



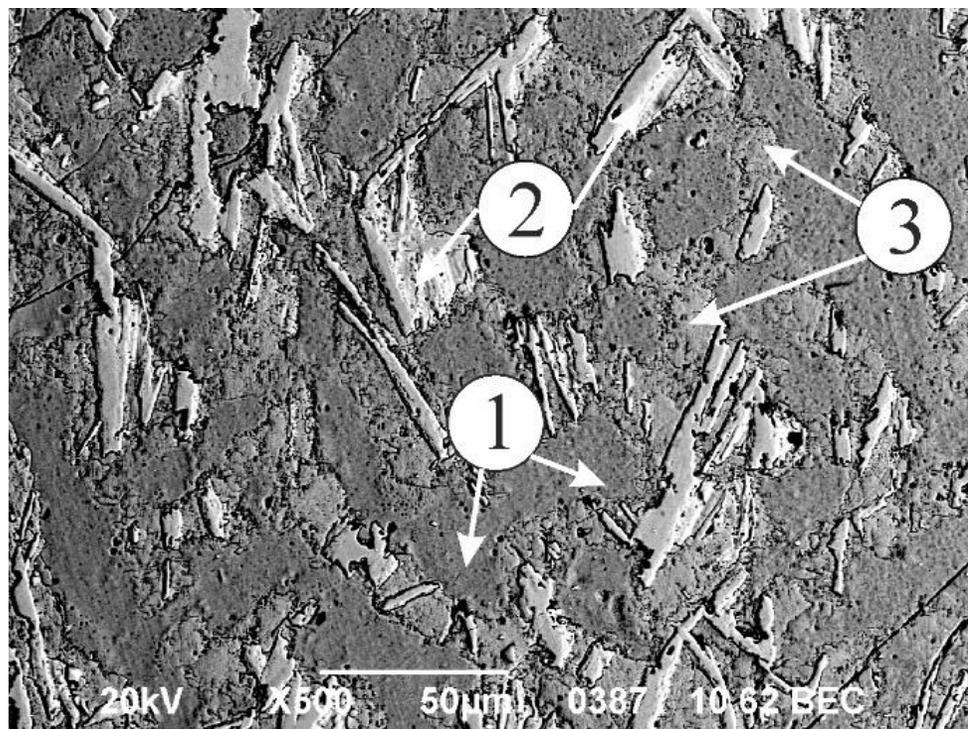
Hysteresis loops of sintered
 SmCo_5 magnets
after HDDR



DR:
1 – 850 °C;
2 – 850 °C, 1 h;
3 – 950 °C

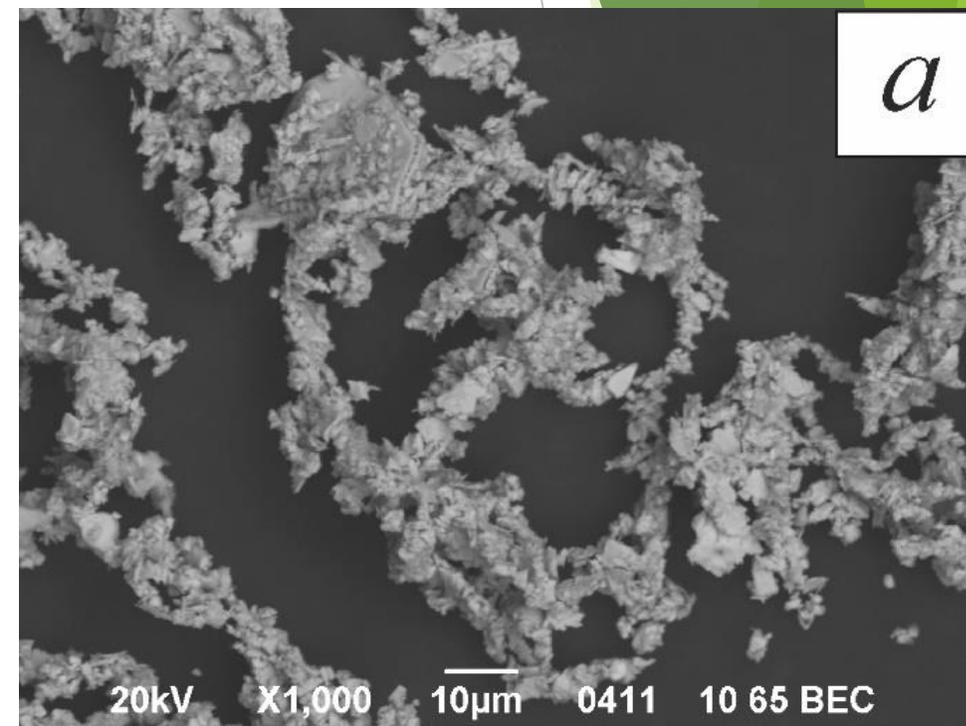
$$\mu_0 H_C \approx 5 \text{ T}$$

Industrial Ferromagnetic $Sm_2(Co,Fe,Zr,Cu)_{17}$ Alloy



Microstructure of the starting alloy:

- 1) $Sm_2(Co,Fe,Zr,Cu)_{17}$ phase,
- 2) $Sm(Co,Fe,Zr,Cu)_5$ phase,
- 3) $Sm_2(Co,Fe,Zr,Cu)_7$ phase

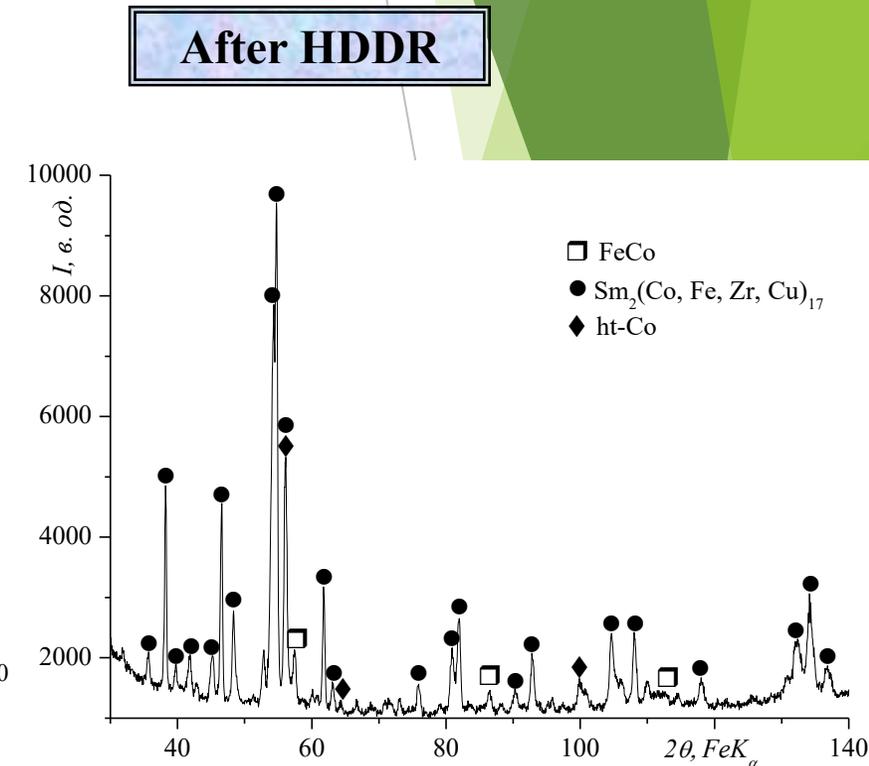
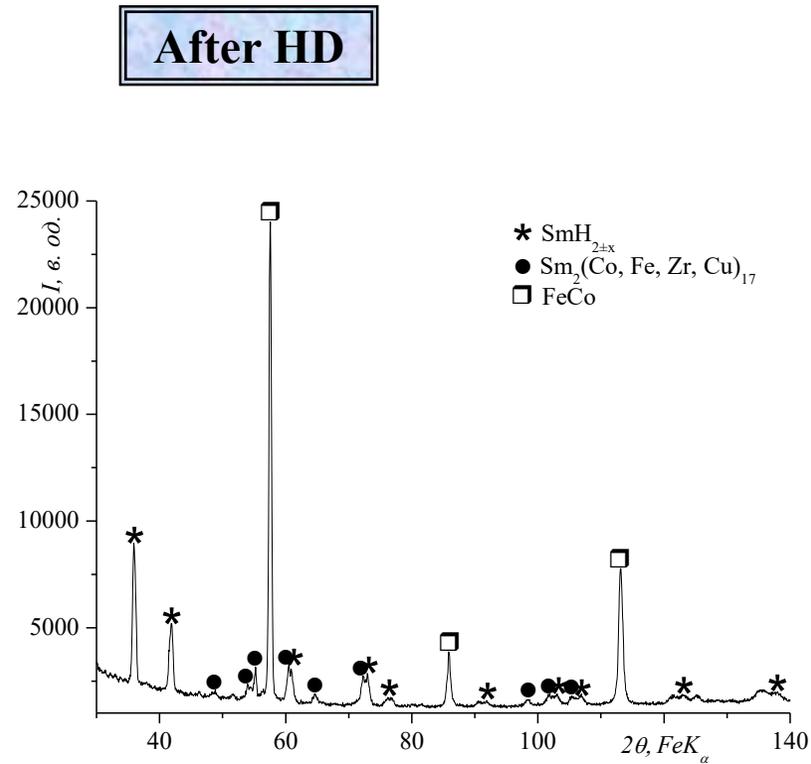
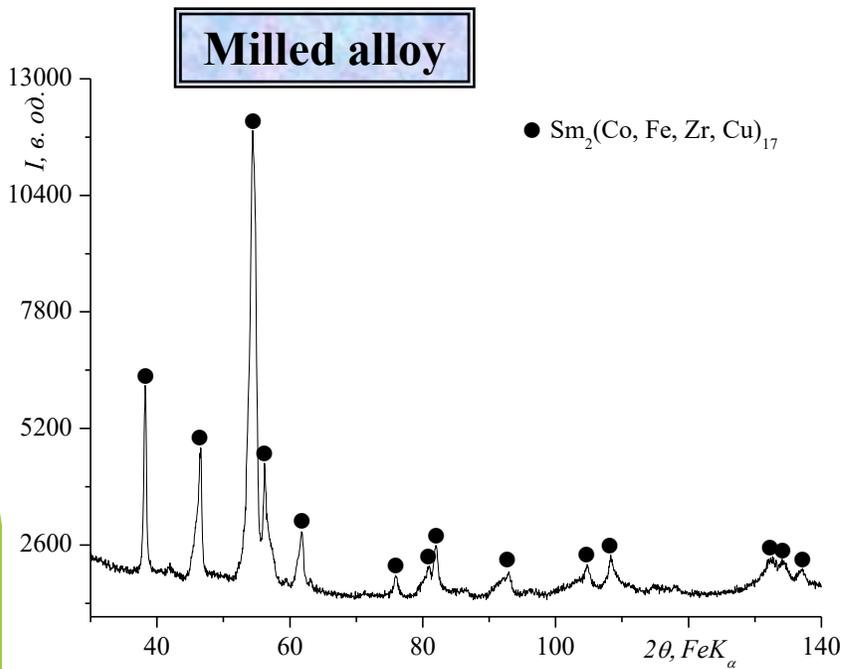


Morphology of the $Sm_2(Co,Fe,Zr,Cu)_{17}$ powder

Industrial Ferromagnetic $Sm_2(Co,Fe,Zr,Cu)_{17}$ Alloy

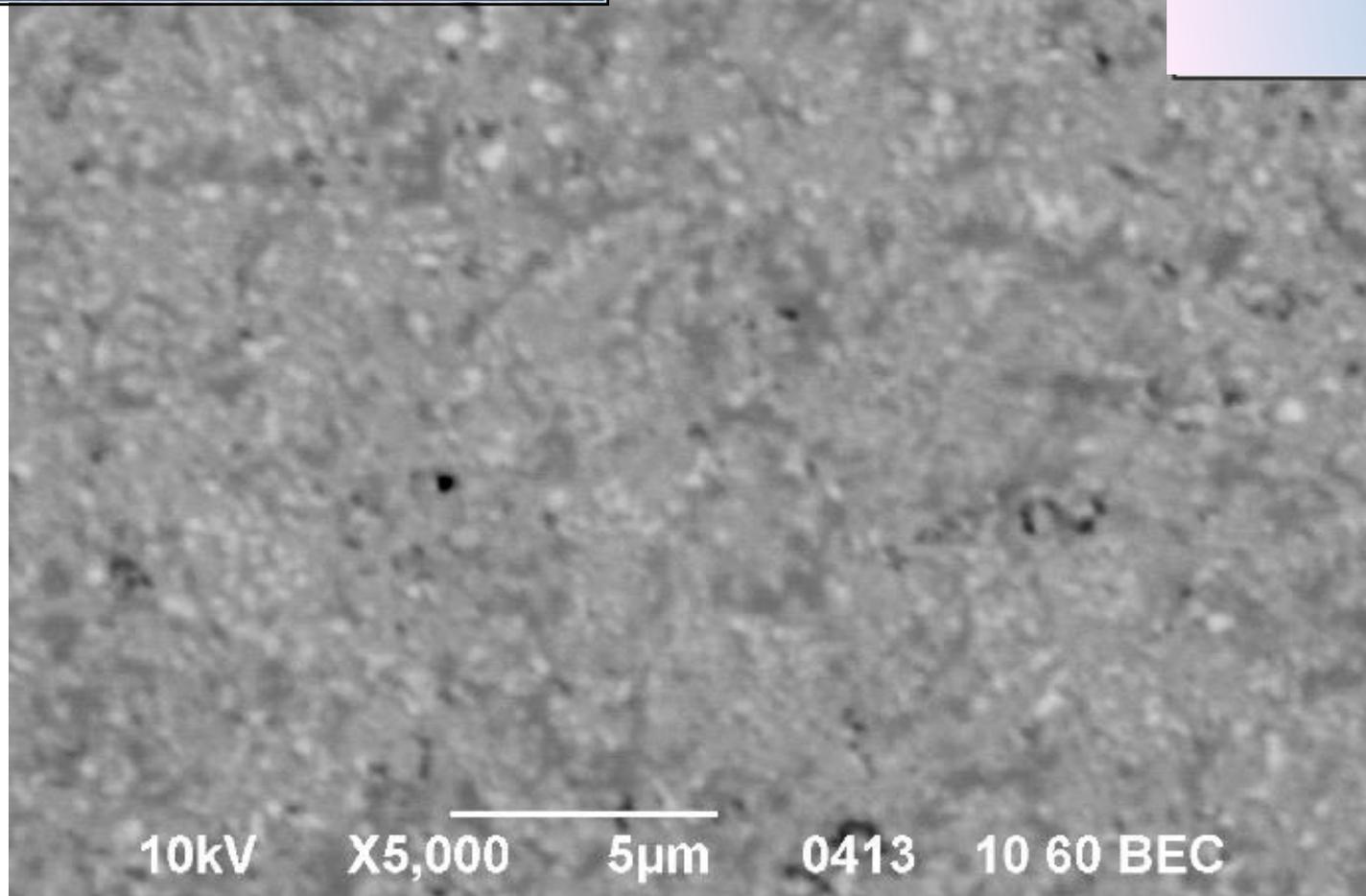
XRD patterns measured for:

The HD stage proceeded at 700°C and DR at 950°C.
Hydrogen pressure of ≤ 1.5 MPa



Industrial Ferromagnetic $Sm_2(Co,Fe,Zr,Cu)_{17}$ Alloy

Microstructure of $Sm_2(Co,Fe,Zr,Cu)_{17}$
alloy sintered by HDDR

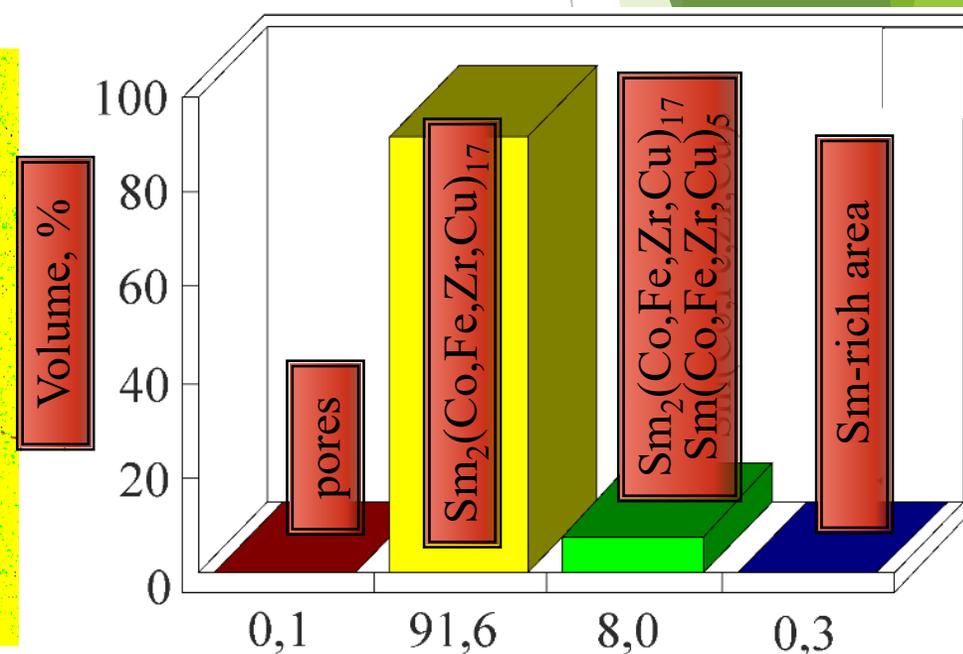
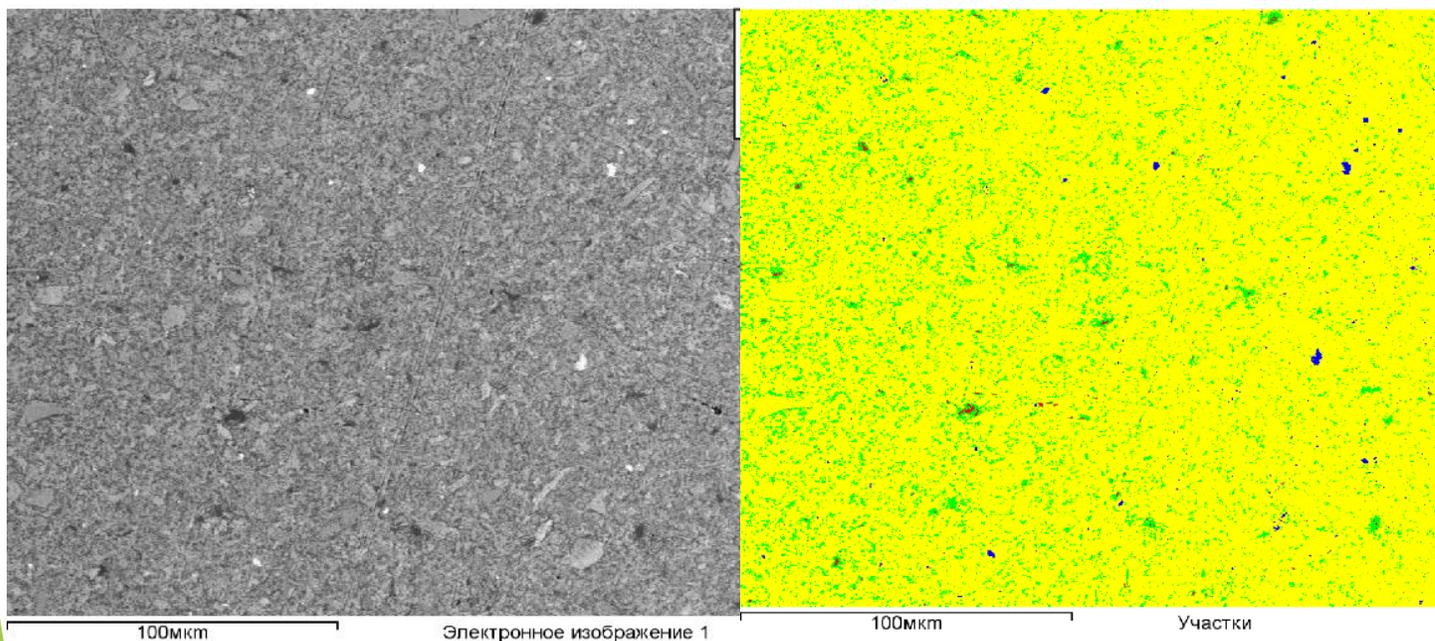


*The HD stage: temperature of 700°C,
hydrogen pressure of ≤ 1.5 MPa
and DR at 950°C.*

Industrial Ferromagnetic $Sm_2(Co,Fe,Zr,Cu)_{17}$ Alloy

The HD stage proceeded at 700°C and DR at 950°C.
Hydrogen pressure of ≤ 1.5 MPa

Quantitative analysis of microstructural components of the $Sm_2(Co,Fe,Zr,Cu)_{17}$ alloy





*Preliminary Results of Sintering $R_2Fe_{14}B$,
 $SmCo_5$ -, and Sm_2Co_{17} Magnetic Materials
Using the HDDR Process*

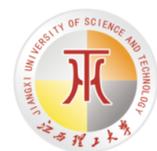
Conclusions

It has been ascertained that $R_2Fe_{14}B$ -, $SmCo_5$ -, and Sm_2Co_{17} -based powders can be sintered in hydrogen at temperatures below 950°C .

The grain sizes of the ferromagnetic phases vary from a few dozens to 300 nm.

The porosity of the sintered materials diminishes with increasing compaction pressure and sintering temperature.

The parameters for producing nanostructured magnets sintered in hydrogen warrant further optimization.



Thank you!