



# Non-magnetic regenerator material of silver oxide for 4 K cryocoolers

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## ABSTRACT

In regenerative cryocoolers, magnetic specific heat is often utilized for heat regeneration at cryogenic temperature, such as below 20 K. Magnetic regenerator materials of rare earth compound which have sufficient specific heat enabled cryocooler to reach below 4 K. However, the magnetic noise emitted from the magnetic materials during the refrigeration cycle affects the performance of noise-sensitive devices. In this study, we propose a non-magnetic regenerator material having “optical phonon degree of freedom” even at cryogenic temperatures, in which silver oxide (Ag<sub>2</sub>O) is selected. Ag<sub>2</sub>O decomposes at temperature above 410 K in ambient atmosphere, whereas we succeeded in fabricating a sintered Ag<sub>2</sub>O bulk and small particles of the size of 0.5 μm with high-density more than 90%. Specific heat measurement down to 100 mK was performed for the sintered bulk sample of Ag<sub>2</sub>O. Below 10 K, a non-Debye behavior was observed, suggesting the contribution from optical phonon modes. Calculation of the phonon density of state (phDOS) performed by the Evolution Strategy algorithm in addition to the first-principles calculation reveals that phDOS has several distinct peaks at low energies, and the low-energy optical phonons contribute to the non-Debye behavior. The low temperature specific heat of Ag<sub>2</sub>O enhanced by the optical phonons is larger than conventional non-magnetic regenerator materials when compared in terms of specific heat per volume. Moreover, the calculation of cooling performance of cryocooler using Ag<sub>2</sub>O particles is found to be reached below 4.2 K. This study shows that non-magnetic material with low temperature specific heat enhanced by optical phonon mode can be used as a regenerator material for regenerative cryocoolers.

## 1. Introduction

Recently, there is a growing interest in application of various types of regenerative cryocooler for quantum computers, superconducting magnets and other cryogenic devices. Among these regenerative cryocoolers, a Gifford-McMahon (GM) cryocooler is comparatively popular and well adopted in various fields. It is designed in the form of multi-stage cooling process to generate a large temperature difference from room temperature (R.T.) to cryogenic temperature. Various regenerator materials, which possess large specific heats under set operating temperatures, are used in both 1st cooling stage and 2nd cooling stage. For example, lead (Pb) and bismuth (Bi) are often used as regenerator materials in the 2nd cooling stage. This is because their Debye temperatures  $\theta_D = 105$  K and 119 K, respectively, are relatively lower than other materials and yet possess large specific heat even at low temperatures. However, as this specific heat produced from the acoustic phonon degree of freedom in accordance with the Debye behavior decreases substantially  $T^3$  law in temperature ( $T \ll \theta_D$ ). Therefore, the lowest

temperature attained by cryocooler using these materials can only go down to lowest  $\sim 5$  K. A new regenerator material was introduced in 1980's, where magnetic specific heat was produced from the electron spin degree of freedom to improve the cooling performance [1–3]. The operating temperature can then go down to as low as 2 K and condensation of He gas has become possible. Currently, regenerator applying both magnetic materials (such as HoCu<sub>2</sub> and Gd<sub>2</sub>O<sub>2</sub>S) and non-magnetic materials such as Bi, is commonly used to achieve the cryogenic temperatures [4,5]. However, there is a setback when using the magnetic regenerator material in which emission of its magnetic noise affects the measurement sensitivity in equipment such as magnetospinography [6], magnetic resonance imaging (MRI) and quantum computer. For this reason, it is desired to develop a magnetic noise free material. We focus on specific heat produced from the “optical phonon degree of freedom” and a non-magnetic material Ag<sub>2</sub>O was selected [7]. The crystal structure of Ag<sub>2</sub>O is a cubic cuprite type with a space group of  $Pn-3m$  (Fig. 1). From the previous studies, it is known that the anharmonic optical phonon mode bends the O-Ag-O link, which is on a straight line in

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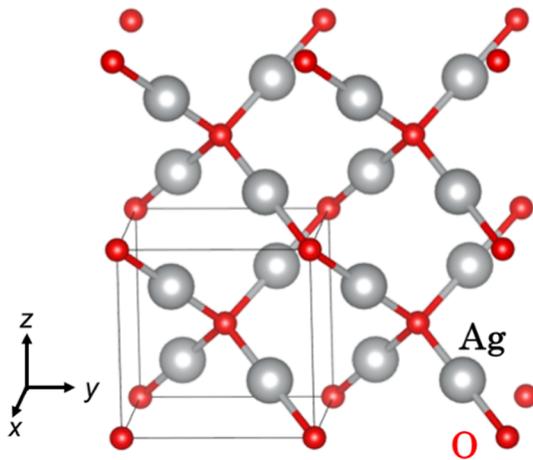


Fig. 1. The crystal structure of  $\text{Ag}_2\text{O}$  is of cubic cuprite type (space group of  $Pn\bar{3}m$ ). The  $\text{Ag}_2\text{O}$  has a linear O-Ag-O link.

ground state [8,9]. The Ag atom with a relative heavy mass, contributes to optical phonon modes at low energies leading to a non-Debye specific heat at low temperatures [10,11]. The regenerator material for GM cryocooler should possess a large specific heat and to be of spherical shape with a size in submillimeter. When forming a spherical particle of  $\text{Ag}_2\text{O}$ , special handling is required to avoid decomposition of  $\text{Ag}_2\text{O}$  into silver and oxygen above 410 K in ambient atmosphere [12,13].

In this paper, we report the spheroidization of  $\text{Ag}_2\text{O}$  in submillimeter and the result of specific heat measurement of  $\text{Ag}_2\text{O}$  down to 100 mK. The temperature dependence of specific heat below 10 K exhibits a non-Debye behavior, suggesting contribution of optical phonon even in at low temperatures. At cryogenic temperature, the  $\text{Ag}_2\text{O}$  exhibits a substantially larger volumetric specific heat than conventional non-magnetic regenerator materials such as Pb and Bi. Moreover, we also succeeded in applying a unique mold sintering to fabricate a spherical particle with a high-density of more than 90% and a diameter of 0.5 mm. Besides, in addition to the first-principles calculation, the Evolution Strategy (ES) algorithm was applied to calculate phDOS from the specific heat measurement data. It is found that phDOS has several distinct peaks at low energies, and these low-energy optical phonons contribute to the non-Debye behavior.

## 2. Experiments

### 2.1. Preparation method of bulk and spherical sample of $\text{Ag}_2\text{O}$

Raw material  $\text{Ag}_2\text{O}$  which is in powder form, of purity greater than 99%, was sintered using the spark plasma sintering (SPS) at 40 MPa at 623 K under vacuum condition for 15 min. The X-ray diffraction (XRD) patterns of both raw material and the sintered bulk sample of  $\text{Ag}_2\text{O}$  were measured by using  $\text{Cu K}\alpha$  radiation source in the  $2\theta$  range from 10 to 80. The XRD patterns shown in Fig. 2 (a) and (b) indicate that both samples have the same cuprite structures. Specific heat of  $\text{Ag}_2\text{O}$  bulk sample was measured at temperature from 100 mK to 300 K, by using the Physical Properties Measurement System (PPMS by Quantum Design, Inc.).

Spheroidization of  $\text{Ag}_2\text{O}$  was performed using three techniques. The first technique used a cross-linking reaction between sodium alginate ( $(\text{NaC}_6\text{H}_7\text{O}_6)_n$  (300 cps) and calcium lactate  $\text{C}_6\text{H}_{10}\text{CaO}_6 \cdot 5\text{H}_2\text{O}$ . In the spheroidization process, the powdery raw material of  $\text{Ag}_2\text{O}$  was mixed evenly with the sodium alginate solution (1 wt%) in a mass proportion of 6:10. The mixture was then injected through a syringe into the calcium lactate solution (5 wt%) to form a spherical  $\text{Ag}_2\text{O}$  (Sol-Gel technique). This continued with the drying process for the spherical  $\text{Ag}_2\text{O}$  in which it was drained and dried in ambient atmosphere. The second technique employed the pseudo isotropic pressure application for the purpose of

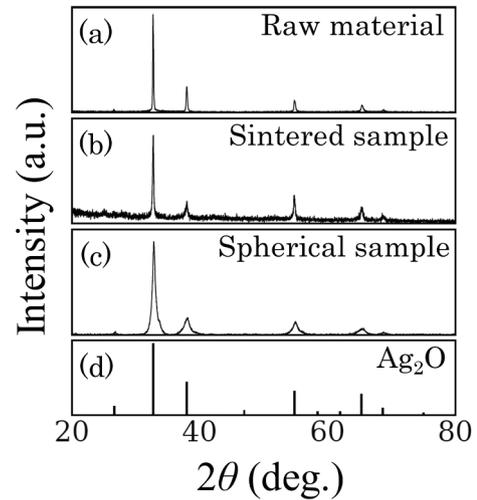


Fig. 2. XRD results of the respective  $\text{Ag}_2\text{O}$  samples (a) raw material, (b) sintered sample by SPS method and (c) spherical sample by mold sintering technique. (d) Calculated XRD pattern of  $\text{Ag}_2\text{O}$ . All these three XRD results display consistent peak patterns with that of the calculated XRD pattern shown in (d).

increasing the bulk density. After the spherical  $\text{Ag}_2\text{O}$  was fully dried under the first technique, it was then put in a pool of zirconia fine particles with diameter of  $\sim 30 \mu\text{m}$  and pressed at 40 MPa at 623 K in a vacuum condition for 15 min (pseudo isotropic pressing technique). The last technique was to apply direct hot press sintering to the powdery raw material of  $\text{Ag}_2\text{O}$  at 40 MPa at 623 K in a vacuum condition for 15 min (mold sintering technique). The spherical  $\text{Ag}_2\text{O}$  was fabricated by using multiple hemispherical microfabricated mold. The mold was pre-coated with a BN release agent for easy removal after the spheroidization process. All three kinds of spherical  $\text{Ag}_2\text{O}$  were confirmed to have the same cuprite structures by the XRD measurement. The XRD pattern of  $\text{Ag}_2\text{O}$  spherical particles prepared by mold sintering technique is shown in Fig. 2 (c). The peak pattern is identical to that of the raw material and the sintered bulk material as shown in Fig. 2 (a) and (b) respectively. This shows that this pattern corresponds to the single phase of  $\text{Ag}_2\text{O}$  with the cuprite structures. Meanwhile, the width of the XRD peak of the spherical particle is wider than those of other samples. This could be caused by microstructural strain or change in crystallite size after the fabrication process. Moreover, all three kinds of spherical  $\text{Ag}_2\text{O}$  particles were then analyzed using the X-ray micro computed tomography scan (TDM1601-II) in order to investigate filling structure within the particle.

### 2.2. Computational details

Cooling power of 4 K cryocooler with a 2nd cooling stage capacity of 1 W using  $\text{Ag}_2\text{O}$  as a regenerator material was calculated at temperature from 4.2 K to 8 K, by REGEN3.3 packages [14]. The typical input

Table 1  
Input parameters for calculation using REGEN3.3.

Parameter	Value
Diameter of particle (mm)	0.5
Diameter of regenerator (mm)	35
Length of regenerator (mm)	140
Hot end temperature of 2nd stage (K)	50
Cold end temperature of 2nd stage (K)	4.2 – 8.0
Frequency (Hz)	1.2
Mass flux at the cold end (g/s)	4.5 – 6.0
Average pressure (MPa)	1.5
Pressure ratio at the cold end	3.2
Thermal conductivity of $\text{Ag}_2\text{O}$ (W/K •m)	0.17 (5 K), 0.31 (10 K), 0.45 (15 K), 0.54 (20 K), 0.93 (40 K), 1.3 (60 K)

parameters for the calculation are listed in Table 1, in which several values are set based on reference from previous study [15].

The pDOS were calculated using two different methods, the first-principles calculation by using the Quantum-ESPRESSO and ALAMODE package, and the Covariance Matrix Adaptation Evolution Strategy (CMA-ES) [16–18]. First-principles calculation were performed with the generalized gradient approximation of density functional theory formulated by the Perdew, Burke, and Ernzerhof [19]. The Norm-Conserving (NC) and Projector-Augmented Wave (PAW) pseudopotentials in standard solid-state pseudopotential libraries (SSSP) were used for Ag and O, respectively [20–24]. Wave function cutoff of 80 Ry and charge density cutoff of 700 Ry were used. The Brillouin zone integrations were performed using Monkhorst-Pack grid of  $k$ -points  $10 \times 10 \times 10$ . The interatomic force constants based on the supercell ( $2 \times 2 \times 2$ ) approach have been calculated by ALAMODE package. The lattice parameter value is 4.811 Å at 0 K in this calculation, while the experimental value at 14 K is 4.745 Å [25]. The CMA-ES is an optimization algorithm that derives an optimum solution even under the presence of multiple local minima, unlike the standard least-square methods. In this paper, this method was used to solve an inverse problem of obtaining pDOS from the specific heat measurement data.

### 3. Results and discussion

#### 3.1. Specific heat and calculated pDOS

Fig. 3 shows the temperature dependence of volumetric specific heat  $C$  ( $\text{J}/\text{cm}^3\text{K}$ ) of the sintered  $\text{Ag}_2\text{O}$  (red dots) and conventional non-magnetic regenerator materials of Pb (blue dash-dotted line) [26] and Bi (black dotted line) [27]. The temperature dependence of specific heat of  $\text{Ag}_2\text{O}$  shows a linear behavior above 2 K, which relates to the non-Debye behavior caused by optical phonons [8]. The specific heat of  $\text{Ag}_2\text{O}$  reaches 6 times larger than that of Pb at 4.2 K, indicating that  $\text{Ag}_2\text{O}$  has a higher advantage as a regenerator material.

In order to investigate the origin of the non-Debye behavior of  $\text{Ag}_2\text{O}$ , we calculated the pDOS of  $\text{Ag}_2\text{O}$  using both ES method and first-principles calculation. Fig. 4(a) and 4(b) show the experimental results and calculations of both temperature dependences of specific heat and pDOS for  $\text{Ag}_2\text{O}$ , respectively. The red and the black solid lines in Fig. 4(a) represent the calculated results by the ES method and the first-principles calculation, respectively. The relation between specific heat  $C_v(T)$  and pDOS  $D(E)$  is expressed as

$$C_v(T) = 9N_A k_B \int_0^\infty D(E) \frac{(\beta E)^2 e^{\beta E}}{(e^{\beta E} - 1)^2} dE, \quad (1)$$

where  $\beta = 1/k_B T$ ,  $k_B$  is Boltzmann constant,  $N_A$  is Avogadro constant. The ES method were repeated until the obtained pDOS reproduced the specific heat measurement. As shown in Fig. 4(b), the results from both ES method and first-principles calculation show similar phonon spectra. It is characterized by the peaks at two regions, that is, one is around 10 meV and the other one is around 60 meV. This is also shown in the result of inelastic neutron scattering measurement at 40 K [9]. Similar spectra were also reported in previous studies [8,11,28,29]. Accuracy of the phonon spectrum calculated by the ES method at low energy region below 10 meV is considered high as it is calculated to fit to the specific heat measurement. On the other hand, the region of around 60 meV, the spectrum of the ES method is different from that of inelastic neutron scattering measurement as shown in Fig. 4(b). This would be due to the absent of specific heat data in the high temperature region ( $\sim 60$  meV). Therefore, in this case, we think that the ES method provide accurate phonon spectra around 10 meV, but the first-principles calculation calculates more accurate for around 60 meV.

#### 3.2. Material spheroidization and calculated cooling performance

In order to put  $\text{Ag}_2\text{O}$  in practical use as a regenerator material, a high-density particle is necessary. Sintering method is often used to fabricate high-density sample in the field of powder metallurgy. However, it is difficult to sinter  $\text{Ag}_2\text{O}$  because it decomposes into silver and oxygen at temperature above 410 K in ambient atmosphere. Therefore, we have tried different approaches in order to obtain the high-density particle. Two types of photographs of each fabricated particle were taken under the optical microscopy in Fig. 5(a)–5(c) and X-ray micro computed tomography (micro-CT) in Fig. 5(d)–5(f). Fig. 5(a) and 5(d) show spherical  $\text{Ag}_2\text{O}$  made by the Sol-Gel technique, the spherical  $\text{Ag}_2\text{O}$  has a diameter of 2.0 mm and a bulk density of  $\sim 25\%$ . The bulk density is calculated based on a true density of  $7.22 \text{ g}/\text{cm}^3$  for  $\text{Ag}_2\text{O}$ . Since the bulk density of the  $\text{Ag}_2\text{O}$  sphere is rather low, the second technique, the pseudo isotropic pressing technique, was applied to continue the spheroidization process. As shown in Fig. 5(b) and 5(e), the sphere then shrunk further to a diameter of 1.5 mm and the bulk density increased to  $\sim 55\%$ . Although the bulk density of  $\text{Ag}_2\text{O}$  sphere has increased, it is still not an ideal bulk density to be used as a practical regenerator material. Furthermore, zirconia particles also remained on the surface of the  $\text{Ag}_2\text{O}$  sphere as shown in Fig. 5(b). To further increase the bulk density, a unique mold sintering technique was employed. We succeeded in fabricating the  $\text{Ag}_2\text{O}$  spherical particle with a diameter of 0.5 mm and a bulk density of more than 90% (Fig. 5(c) and 5(f)). In addition to that, a thin layer of silver (Fig. 5(c)) formed on the surface of  $\text{Ag}_2\text{O}$  after the fabrication was found. The existence of the thin silver would increase the abrasion resistance against vibration occurred during the cryocooler operation.

Since we have succeeded in fabricating the  $\text{Ag}_2\text{O}$  particle with an ideal density as a practical regenerator material, we then utilized the properties of the  $\text{Ag}_2\text{O}$  particle to calculate the cooling power of the 2nd stage in GM cryocooler between 4.2 K and 8 K. For comparison purpose, the cooling power using the conventional non-magnetic regenerator materials Pb and Bi were also calculated. In the calculation, the diameter of particle of these materials is fixed at 0.5 mm. Fig. 6 shows calculated cooling power for  $\text{Ag}_2\text{O}$ , Pb and Bi particles used in the cryocooler at different temperatures. For  $\text{Ag}_2\text{O}$  particles, the cooling power remains even at 4.2 K. On the other hand, for Pb and Bi particles, their lowest temperatures can only go down to around 6 K and 7 K, respectively. These results indicate that the large volumetric specific heat of  $\text{Ag}_2\text{O}$  shown in Fig. 3 originating from the optical phonon mode based on the pDOS (Fig. 4(b)) contributes to reach temperatures below 4.2 K. We

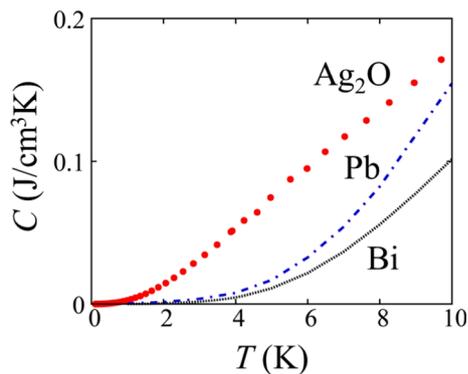
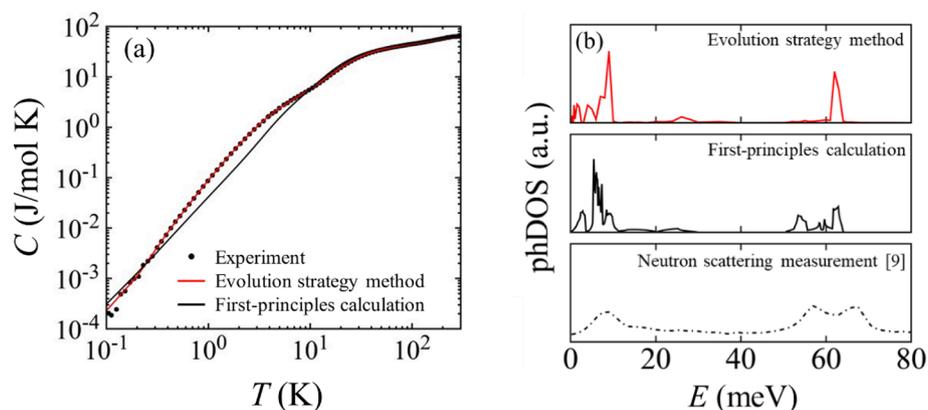
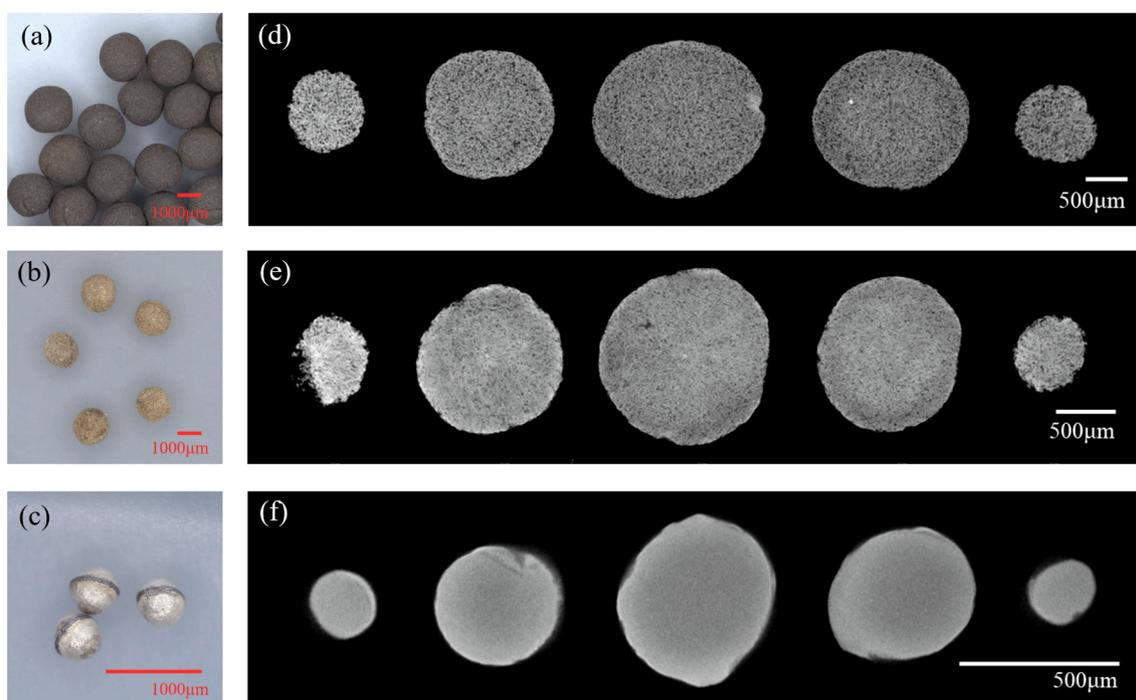


Fig. 3. Temperature dependence of volumetric specific heat  $C$  ( $\text{J}/\text{cm}^3\text{K}$ ) of the sintered  $\text{Ag}_2\text{O}$  (red dots), conventional non-magnetic regenerator materials of Pb (blue dash-dotted line) [26] and Bi (black dotted line) [27].  $\text{Ag}_2\text{O}$  has a larger specific heat than Pb and Bi at cryogenic temperature. The temperature dependence of specific heat of  $\text{Ag}_2\text{O}$  shows a linear behavior due to its optical phonon (non-Debye behavior). (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)



**Fig. 4.** (a) Experimental and calculated results of specific heat of  $\text{Ag}_2\text{O}$  in logarithmic form. Experimental results are represented by the black dots. The red solid line and black solid line represent fitted result by the ES method and calculated result by the first-principles calculation, respectively. (b) The phDOS calculated by the ES method shows similar peaks to that of calculated by first-principles calculation and inelastic neutron scattering measurement at 40 K [9]. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)



**Fig. 5.** (a)-(c) Photographs taken by optical microscopy. (a)  $\text{Ag}_2\text{O}$  spheres made by Sol-Gel technique, with a diameter of 2.0 mm and bulk density of  $\sim 25\%$ . (b)  $\text{Ag}_2\text{O}$  spheres made by pseudo isotropic pressing technique, with a diameter of 1.5 mm and the bulk density of  $\sim 55\%$ . (c)  $\text{Ag}_2\text{O}$  spheres made by the mold sintering technique, with a diameter of 0.5 mm and bulk density of 90% and above. (d)-(f) Series of images taken by the X-ray micro-CT, which display different degree of bulk density of the three spheres respectively.

also found that the cooling performance increases as the diameter of the particle decreases [30]. Smaller particle facilitates better heat exchange with He gas.

#### 4. Summary

In this paper, the study covers both experimental and theoretical perspective of  $\text{Ag}_2\text{O}$  as a non-magnetic regenerator material with specific heat produced from “optical phonon degree of freedom”. The specific heat of  $\text{Ag}_2\text{O}$  was measured and shows a non-Debye behavior at low temperatures, indicating optical phonon modes exist at low energy regions. At temperature below 10 K, the specific heat of  $\text{Ag}_2\text{O}$  is larger comparing to that of other two conventional regenerator materials, Pb and Bi, by the contribution of the optical phonon modes. To investigate

the origin of the non-Debye behavior, both ES method and first-principles calculation were performed to calculate the phDOS. These results indicate that the phonon peaks around 10 meV contribute to the large specific heat of  $\text{Ag}_2\text{O}$  in cryogenic temperatures. Furthermore, we succeeded in applying a mold sintering technique to fabricate a  $\text{Ag}_2\text{O}$  particle of 0.5 mm in diameter and a density of more than 90%, which is practical to be used in regenerative cryocooler. The calculated cooling power of cryocooler using properties of the  $\text{Ag}_2\text{O}$  particle also shows that its lowest temperature can reach below 4.2 K. This feasibility study indicates that the concept to adopt a non-magnetic material with optical phonon degree of freedom as a regenerator material at cryogenic temperature can be realized.

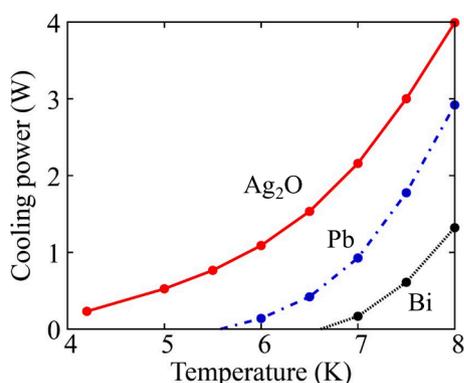


Fig. 6. Calculated cooling power of 2nd stage in GM cryocooler using regenerator materials  $\text{Ag}_2\text{O}$ , Pb, and Bi at different temperatures. The cooling power of cryocooler with  $\text{Ag}_2\text{O}$  remains even at 4.2 K.

### CRediT authorship contribution statement

**Sotaro Nishioka:** Data curation, Formal analysis, Investigation, Methodology, Software, Visualization, Writing – original draft. **Shinji Masuyama:** Software, Writing – review & editing. **Akiko T. Saito:** Conceptualization, Investigation, Funding acquisition, Project administration, Supervision, Writing – review & editing.

### Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

### Data availability

The availability will be considered on a case-by-case basis.

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